# 2024 Annual Geotechnical Inspection – Doris Tailings Impoundment Area

Hope Bay Mine, Nunavut, Canada Agnico Eagle Mines Limited



SRK Consulting (Canada) Inc. • CAPR003066 • March 2025



#### 2024 Annual Geotechnical Inspection - Doris Tailings Impoundment Area

Hope Bay Mine, Nunavut, Canada

#### Prepared for:

Agnico Eagle Mines Limited 145 King Street East, Suite 400 Toronto, ON, Canada M5C 2Y7

+1 416 947 1212 www.agnicoeagle.com

#### Prepared by:

SRK Consulting (Canada) Inc. 2600–320 Granville St. Vancouver, BC V6C 1S9 Canada

+1 604 681 4196 www.srk.com

Lead Author: Peter Luedke, PEng Anton Novikov, EIT AN Reviewer: Megan Miller MEng, PEng Initials: MMM 

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South Dam helicopter overview from a helicopter during 2024 AGI

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## **Executive Summary**

Hope Bay is an advanced exploration site and former operating mine in care and maintenance owned by Agnico Eagle Mines Ltd. (Agnico Eagle). Hope Bay comprises three distinct areas of known mineralization, Doris, Madrid (North and South), and Boston. Before the site transitioned into care and maintenance in 2021, the Doris Mine (Phase 1) was in operation under Nunavut Water Board (NWB) Type A Water License 2AMDOH1335 - Amendment No.2. This license covers the current Phase 1 and well as the Phase 2 mining developments. Agnico Eagle contracted SRK Consulting (Canada) Inc. to conduct an annual geotechnical inspection (AGI) for the Tailings Impoundment Area (TIA) in accordance with all stipulated license conditions, NWB Water Licence 2AM-DOH1335 Part I, Item 9 and 10.

The TIA currently consists of a water retaining dam, the North Dam, and a tailings retaining dam, the South Dam and the Interim Dike. Subaerial tailings are currently retained by the South Dam, the Reclaim Pond is impounded by the North Dam and the Saline Pond is segregated from the Reclaim Pond by the Interim Dike. The North Dam was constructed during the winters of 2011 and 2012, Phase 1 of the South Dam was constructed in one season during the 2017/2018 winter season, and the Interim Dike was constructed in the winter of 2023.

Section 5 provides a summary of the 2024 AGI inspection components for the TIA, and the recommendations following the site inspection and subsequent review of monitoring data. Based on the results of the AGI in September 2024, the North Dam and South Dam are functioning as designed, and no significant concerns were identified regarding the ongoing performance of these structures. The Interim Dike is also performing adequately, with some recommended improvements. There are maintenance items that require attention, and suggestions for improvement of the performance and safety of the TIA and should be addressed.

# 1 Introduction

## 1.1 General

Hope Bay is both an advanced exploration project of Agnico Eagle Mines Ltd. (Agnico Eagle) and a previously operating mine site currently in care and maintenance. The site is located 705 km northeast of Yellowknife and 153 km southwest of Cambridge Bay in Nunavut Territory and is situated east of Bathurst Inlet (Figure 1). The site comprises three distinct areas of known mineralization, Doris, Madrid (North and South), and Boston.

Construction of the Tailings Impoundment Area (TIA) began in 2010 with the North Dam. Commercial production and tailings deposition within the TIA began in 2017. The South Dam, which provides the southern tailings containment, was constructed in 2018, prior to the development of the existing tailings beach. In order to segregate saline mine water and reclaim water, the Interim Dike was constructed in 2023 to replace the temporary Aquadam.

An annual geotechnical inspection (AGI) of the TIA containment dams and supplementary infrastructure including the Interim Dike, pipelines and emergency catch basins is required to fulfill NWB Water Licence 2AM-DOH1335 Part I, Item 9 and 10. Therefore, Agnico Eagle contracted SRK Consulting (Canada) Inc., the Design Engineer, to conduct the 2023 annual geotechnical inspection. SRK has conducted all formal AGI for the TIA since it was constructed, and SRK held the role of Engineer of Record for the TIA infrastructure from 2011 to the end of 2021.

Peter Luedke, PEng, Senior Consultant assisted by Anton Novikov, EIT, Staff Consultant with SRK conducted the on-site annual geotechnical inspection between September 11 and 18, 2024, accompanied by Agnico Eagle's Site Geotechnical Engineer (Brennan Jay, EIT). Weather conditions during the inspection were sunny to overcast. The detailed inspection of the dams and supporting infrastructure was carried out on foot, followed by a low-altitude helicopter flyover for an aerial reconnaissance of the TIA. A post-inspection meeting was held on-site with key personnel from relevant departments, where SRK presented the preliminary inspection findings.

Monitoring and surveillance activities occur on a regular basis throughout the year (Section 4.1), with Agnico Eagle and SRK working in close collaboration to review the data and make management decisions based on the data and overall performance of the TIA. The TIA monitoring data is summarized within this AGI report. To align the data included in the AGI report with the site inspection, the primary focus of monitoring data review is from October 1 to September 30, 2024 (the monitoring year), unless otherwise stated.

This report provides a summary of the conditions observed during the site inspection, a review of monitoring data, and recommendations to support the ongoing successful performance of the tailings management system. Photos detailing the inspection conditions are included as photologs, and a comprehensive review and analysis of the monitoring data are provided in the appendices.

## 1.2 Inspection Requirements

Under Type A Water License 2AM-DOH1335 – Amendment No. 2, dated December 7, 2018, the specific TIA inspection requirements are stated in Part I, items 9 and 10 of the license:

9. The Licensee shall undertake a geotechnical inspection of all surface infrastructure and earthworks, annually between July and September, by a Geotechnical Engineer. The inspection shall be conducted in accordance with applicable best practices including the Canadian Dam Association Guidelines for water and waste containment facilities.

10. The Licensee shall submit to the Board for review, within ninety (90) days of completion of the geotechnical inspection, a report in accordance with Part I Item 9 and/or the Annual Report. The report shall include a cover letter from the Licensee outlining an implementation plan addressing each of the Geotechnical Engineer's recommendations and shall include the following:

- a. All quantities in cubic meters of dike seepage from the North, West, and South Dams pumped back into the Tailings Impoundment Area;
- *b.* As-built drawings and a summary of the mitigation works undertaken along the shoreline of the Tailings Impoundment Area in response to erosion; and
- c. All data and information generated from the monitoring of all project geotechnical instrumentation.

It should be noted that the report associated with the geotechnical inspection described above is routinely submitted to the Nunavut Water Board on an annual basis as part of the Hope Bay Annual Report.

# 2 Site Conditions

## 2.1 Tailings Impoundment Area History

A summary of the TIA permitting, construction, and operations history is provided in Table 2-1.

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Period	Comments
Winter 2011 and Winter 2012	North Dam constructed (SRK 2012b).
Fall 2012	Project placed into Care and Maintenance before any tailings are produced.
2012 – 2015	Project in Care and Maintenance.
January 2017	Start of tailings deposition in TIA.
January – June 2018	Completion of South Dam Phase 1 construction.
August 2018	Commissioning of additional instrumentation at the South Dam.
May 2019	Instrumentation upgrades and additional datalogger installations at the South Dam.
February 2020	Doris TIA discharge via the Roberts Bay Discharge System begins. System temporarily offline starting August 2020 to May 2021, December 2021 to July 2022, January to April 2023.
October 2021	Doris Mill is shut down (put in Care and Maintenance), and tailings deposition ceases.
January 1, 2022	Agnico Eagle and TMAC amalgamated and continued under the Agnico Eagle name
January 1, 2022	Doris TIA EOR role transitioned from SRK to Agnico. SRK assumes the role of Design Engineer.
June 2022	The reclaim pump pad and associated reclaim pumps were moved onto the shoreline to the north after decommissioning the previous Reclaim Jetty.
July 2022	Aquadam constructed within the TIA as part of the site water management strategy. Saline water intercepted by the Doris underground is discharged to the south of the Aquadam. The purpose of the Aquadam is to segregate saline water in the south of the TIA from water to the north that is discharged to Roberts Bay.
March – June 2023	Interim Dike was constructed to replace the Aquadam with a more robust structure. The purpose of the Interim Dike is similar to the Aquadam, to segregate saline water in the south of the TIA from the Reclaim Pond to the north.
April – June 2023	The South Dam toe berm is constructed along the downstream side of the South Dam.
May 2023	Emergency Water Treatment Plant (EWTP) constructed and commissioned.
November 2023	Upstream ground temperature cables installed.
July 2024	Passive thermosyphons converted to hybrid thermosyphons

Table 2-1: Summary of TIA Development History

## 2.2 Tailings and Water Management Overview

The tailings impoundment area (TIA) is located southeast of the Doris mill and mine (Figure 1 and 2). Containment for the TIA is provided through a water-retaining frozen core dam (North Dam) which retains the Reclaim Pond, and a geosynthetic clay liner (GCL) lined frozen foundation tailings dam

(South Dam) which retains the tailings beach. The current tailings capacity of the TIA is approximately 2.5 Mt of subaerially deposited tailings.

The permitted Phase 2 TIA has not yet been constructed. The Phase 2 TIA increases the overall tailings solids containment capacity to approximately 18 Mt (SRK 2017e). The Phase 2 expansion will include a raise of the South Dam and a new West Dam (also a frozen foundation GCL lined dam) (Figure 3).

The TIA reclaim pond is used as the overall collector for all site surface contact water, which is either pumped or trucked to the TIA. Since July 2022, saline underground water has been segregated into the southern portion of the TIA in the Saline Water Storage (SWS), which is a separate cell retained by the Interim Dike. When possible, saline water is discharged to Roberts Bay. Water in the Reclaim Pond is typically made up of freshwater runoff and recycled for processing make-up during operations, however, under Care and Maintenance, water is discharged to Roberts Bay by the Roberts Bay Discharge System (RBDS) via the water treatment plant or directly discharged when water quality allows. Prior to discharge to Roberts Bay, all water must meet Metal and Diamond Mining Effluent Regulations (MDMER) limits. The water storage capacity of the Reclaim Pond varies over the mine life but is greater than 6.4 Mm<sup>3</sup> in 2024.

As part of the TIA design (SRK 2017e) and as detailed in the OMS manual (AEM 2024) the water level is expected to be managed through regular discharges to Roberts Bay. Due to the substantive freeboard and design capacity to contain the Probable Maximum Flood (PMF), and as such no spillway was included in the design. A review of the operational beach slopes and tailings deposition plan (SRK 2021a) indicates current deposition plan will decrease the Reclaim Pond capacity over time. During the later stages of the currently permitted facility, the capacity of the Reclaim Pond will be reduced to between 133,000 m<sup>3</sup> and 209,000 m<sup>3</sup>. Until the North Dam is breached at closure, the inflow design flood (IDF) storage volume is greater than 640,000 m<sup>3</sup> and requires adequate control in accordance with CDA (2019). To mitigate against the risk of an overtopping failure at the North Dam and to remove the dependency on an active discharge a Emergency Overflow Channel (EOC) has been designed and is planned to be constructed when tailings deposition resumes. A discharge from the EOC would only occur during a very low probability emergency event and would not occur under normal operating conditions.

Assuming the Roberts Bay discharge system continues to be operational and adequate discharge occurs, it is not until the last two to four years of the tailings deposition (depending on operational pond volumes) that the available pond storage in the TIA is expected to fall below the IDF storage volume requirement. At that point in time, it is expected that lowering the elevation of the TIA's maximum normal operating water level (NOWL) will be required to contain the IDF storm event.

A detailed review of the water and load balance is provided annually under a separate cover (SRK, 2025).

The permitted tailings production rates and associated tailings storage requirements for the Doris TIA are summarized in Table 2-2.

Description	Value
Nominal Tailings Production Rate (Design)	4,000 tonnes per day (tpd) <sup>1</sup>
Tailings Specific Gravity	2.85
Deposited Tailings Dry Density	1.3 t/m <sup>3</sup>
Tailings Solids Content	35% solids (by weight) initially, increasing to 65% (dependent on mine water management during operations)
Total Tailings Storage Requirement:	
By Mass	18.0 Mt
By Volume	13.9 Mm <sup>3</sup>
Remaining Tailings Storage Requirement:	
By Mass	16.1 Mt
By Volume	12.4 Mm <sup>3</sup>
Ice Entrainment Allowance:	
Percentage of Tailings Capacity	20%
By Volume	2.4 Mm <sup>3</sup>
Tailings Beach Slope:	Between 0.5% and 1.0%

#### **Table 2-2: TIA Design Volumes and Parameters**

Notes:

<sup>1</sup> The operation is currently in Care and Maintenance.

## 2.3 Tailings Impoundment Area Infrastructure

## 2.3.1 North Dam

The North Dam forms the northern boundary of the Doris TIA within a narrow natural valley, blocking the original Tail Lake outlet to Doris Lake (Figure 3). The North Dam impounds the Reclaim Pond and was designed as a water retaining structure. The dam has a central frozen core with a secondary upstream Geosynthetic Clay Liner (GCL). The dam is constructed from local quarry rock and consists of processed fines for the core, 150 mm transition material, and a run of quarry (ROQ) outer shell. To ensure maintenance of the frozen foundation and frozen core conditions, the key trench of the dam is equipped with 12 horizontal thermosyphon evaporators to cool the foundation of the key trench (SRK 2007, 2012a, 2013a, 2015a). As of July 2024, the thermosyphons have been converted from passive thermosyphons to hybrid thermosyphons. The hybrid system utilizes passive cooling during the winter (when ambient air temperatures are below the ground temperature), and active cooling during warmer ambient air temperature. The passive thermosyphons function when the ambient air temperature is colder than the ground temperature where the thermosyphon is located. This happens because of the phase change of the carbon dioxide gas with which the thermosyphon is filled. Therefore, during the winter months, the cold ambient air temperature is used to draw heat from the foundation. When the ambient air temperature rises, the active thermosyphon cooling system is activated which utilizes mechanical cooling at the thermosyphon riser to continue the heat exchange cycle through the warmer seasons. Figure 4 through Figure 6 depict pertinent details of the North Dam and its instrumentation.

Construction of the North Dam started in February 2011 and was completed in April 2012, over two distinct winter seasons, as-built details are provided in SRK (2012b).

## 2.3.2 South Dam

The South Dam is located at the southern end of the former Tail Lake, on the watershed divide toward Ogama Lake (Figure 3). The South Dam is designed as a frozen foundation dam consisting of a compacted rock fill embankment (sourced from a local quarry) with a GCL keyed into the permafrost overburden and bedrock foundation for seepage control. Design parameters and design criteria are summarized in Table 2-3 and Table 2-4 respectively, with Figure 7 through Figure 9 presenting pertinent details of the South Dam design. The dam is designed to retain beached tailings as opposed to water. The dam construction occurs in two phases, the Phase 1 dam has been constructed and the Phase 2 dam is a future downstream raise.

South Dam construction began in January 2018 and Phase 1 construction was completed in June 2018. The South Dam instrumentation was commissioned in August 2018, with additional instrumentation installed in 2019.

In 2023, the South Dam toe berm was constructed. The toe berm is constructed of run-of-quarry rock fill and is typically 2.2 meters thick and 7 meters wide from the downstream slope of the dam to the crest of the toe berm. The intent of the toe berm is to mitigate the tension cracking previously observed on the downstream slope of the South Dam, specifically within the lateral extent of the existing tailings beach. The toe berm makes up a portion of the Phase 2 South Dam embankment, the remainder of which has not yet been constructed.

## 2.3.3 West Dam

The design for the West Dam is a frozen foundation dam with a key trench and a GCL liner keyed into permafrost, similar in design to the South Dam. It is intended to retain future beached tailings along low-lying ground on the western perimeter of the TIA (Figure 3).

If and when required to contain future tailings, this dam will be constructed in a single stage using local quarry rock.

## 2.3.4 TIA Design Parameters and Design Criteria

Geometric design parameters and design criteria for each dam are provided in the OMS Manual, and summarized in Table 2-3 and Table 2-4 for ease of reference.

Description	North Dam	South Dam	West Dam
Structure Type	Frozen core rock fill dam with geomembrane	Frozen foundation rock fill dam with geomembrane	Frozen foundation rock fill dam with geomembrane
Retains	Water	Tailings	Tailings
Secondary Seepage Barrier	GCL	GCL	GCL
GCL Deployment Slope	2.5H:1V	Phase 1 – 3H:1V Phase 2 – 4H:1V	3H:1V
Thermosyphons	12 sloped	None	None
Crest Centerline Length	220 m	515 m	470 m
Maximum Height	11.0 m	Phase 1 – 6.0 m Phase 2 – 14.0 m	5.0 m
Crest Elevation	37.5 masl	Phase 1 – 38.0 masl Phase 2 – 46.0 masl	46.0 masl
Core/GCL Elevation	35.0 masl	Phase 1 – 37.0 masl Phase 2 – 45.0 masl	45.0 masl
Full Supply Level (FSL)	33.5 masl	Phase 1: Water – 33.5 masl Tailings – 36.5 masl Phase 2: Water – 33.5 masl Tailings – 44.5 masl	Water – 33.5 masl Tailings – 44.5 masl
Original Tail Lake Water Level	28.3 masl		
Total Actual Freeboard (Crest to FSL)	4.0 m	Phase 1: Water – 4.5 m Tailings – 1.5 m Phase 2: Water – 12.5 m Tailings – 1.5 m	Water – 12.5 m Tailings – 1.5 m
Total Actual Minimum Freeboard (Core/GCL to FSL)	1.5 m	Phase 1: Water – 3.5 m Tailings – 0.5 m Phase 2: Water – 11.5 m Tailings – 0.5 m	Water – 11.5 m Tailings – 0.5 m
Required Normal Freeboard (CDA 2013)	Wind setup (0.07 m) +	Wave runup (1.06 m) = 1	l.13 m
Required Minimum Freeboard (CDA 2013)	CDA Wind setup (0.06 m) + Wave runup (1.16 m) = 1.22 m Inflow Design Flood (IDF) Freeboard = 2.1 m (at end of mine life w Reclaim Pond is at its minimum size)		I.22 m t end of mine life when
Thermal Protection above Frozen Core	2.5 m	n/a	n/a
Crest Width	13 m	10 m	10 m
Upstream Structure Slope	6H:1V	4H:1V	4H:1V

Table	2-3:	TIA	Containment	Dams	<b>Geometric Design</b>	Parameters
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Description	North Dam	South Dam	West Dam
Downstream Structure Slope	4H:1V	2H:1V	2H:1V
Key Trench Depth	Varies (2.0 – 5.0 m)	Varies (2.0 – 4.0 m)	4.0 m
Key Trench Upstream Slope	0.5H:1V	2H:1V	2H:1V
Key Trench Downstream Slope	0.5H:1V	1H:1V	1H:1V

#### Table 2-4: TIA Containment Dams Design Criteria

Description	North Dam	South Dam	West Dam	
Settlement Allowance				
Foundation thaw of 1 m (partial thaw)	1.00 m	0.47 – 0.67 m	0.40 – 0.60 m	
Foundation thaw of 7 m (full thaw)		2.45 – 3.85 m	2.03 – 3.43 m	
Deformation Allowance (Total Strain due to Creep)	<2%	n/a	n/a	
Design Life:				
Active use as water retaining structure				
Design basis as water retaining structure	17 years			
Design basis until breach	22 years			
Active use as solids retaining structure	30 years	17 years	17 years	
Design basis as solids retaining structure		25 years	25 years	
Annual Exceedance Probability (AEP) for Inflow Design Flood (IDF)				
Risk Based	1/2,475 (0.0004)	)		
Standards Based	1/3 between 1/1	,000 and the PMF <sup>(</sup>	1)	
	1.3 during const	ruction		
Static Stability Factor of Safety: Long-term (Drained	1.5 during operation and closure			
	1.2 to 1.3 partial	or rapid drawdown	า	
Decude Static Stability Easters of Safety	1.0 during earth	quake		
	1.2 post earthqu	ake		
AEP for Earthquake Design Ground Motion	1/2,475 (0.0004)			
Peak Ground Acceleration (PGA)	0.060g <sup>(2)</sup>	0.036g	0.043g	
Mean Annual Air Temperature Climate Change	+6.8°C up to yea	ar 2100		
Thermal Design Criteria (Normal Conditions) <sup>(3)</sup>				
Foundation	-8°C	-2°C	-2°C	
Frozen core (thermal block zone)	-2°C	n/a	n/a	
Tailings Freezing Point Depression	n/a	0 to -1°C	0 to -1°C	
Seepage Allowance	78 m³/day	50 m³/day	<1 m³/day	

Notes:

<sup>1</sup> Value based on experiential engineered judgement.

<sup>3</sup> This value is the design criteria used during the design of the structure. Refer to the current TIA OMS manual for operating criteria and trigger levels (AEM 2024).

<sup>&</sup>lt;sup>2</sup> A peak ground acceleration for a 1/2,475 return period was not available at the time of design of the North Dam, and therefore the PGA of 0.06 g was selected based on published data for Kugluktuk. This is further described in SRK (2007).

### 2.3.5 Interim Dike

The Interim Dike was constructed between March and June 2023. The structure is fully within the current TIA footprint and was constructed upstream (south) of the former Aquadam location. The Interim Dike is designed as an interim structure to segregate saline underground mine water from the overall Reclaim Pond, as part of the updated water management strategy during Care and Maintenance.

The structure consists of two parallel rock berms, with a compacted tailings core and a GCL liner on the interior face of the northern berm to provide additional hydraulic control. The upstream pond is actively controlled by pumping, and if required, passively controlled by a water elevation control channel (WECC).

A summary of the Interim Dike dimensions is provided in Table 2-5, additional information is provided in the construction summary report (AEM 2024):

Description	Interim Dike
Structure Type	TIA Internal Dike
Secondary Seepage Barrier	GCL
GCL Deployment Slope	2.5H:1V
Crest Centerline Length	300 m
Maximum Height	3.9 m (as-built)
Hydraulic Control Elevation (Crest along GCL)	34.9 masl (as-built)
WECC Invert / Activation Elevation	34.3 masl (as-built)
Normal Operating Water Level (South Pond) (NOWL)	34.0 masl
Minimum Freeboard (WECC Invert to NOWL)	0.3 m
Crest Width	50 m (Varies)
Upstream Structure Slope	2H:1V
Downstream Structure Slope	2H:1V
Key Trench Depth	1.0 m (Typical – Varies)
Key Trench Upstream Slope	0.5H:1V
Key Trench Downstream Slope	0.5H:1V

#### Table 2-5: Interim Dike Geometric Design Parameters

## 2.3.6 Tailings Deposition System

The mine is currently in Care and Maintenance and therefore the tailings discharge system is inactive. Prior AGIs (SRK 2018a, 2019a, 2020a, 2021b) describe the design and history of beach development.

Prior to entering Care and Maintenance and the cessation of mill operation (October 2021), a cumulative 1,857,159 tonnes of tailings solids were deposited into the TIA.

## 2.3.7 Emergency Dump Catch Basins

Two Emergency Dump Catch Basins (EDCBs) have been constructed on either side of Doris Creek (Figure 2). The EDCBs are lined cells constructed at a topographic low-point along the tailings and reclaim pipeline routes that allow for the pipelines to be drained during prolonged mill shutdowns or power failures to prevent pipeline freeze-up. They were designed to accommodate at least two consecutive shutdowns plus direct precipitation over the basin areas. The EDCBs were constructed in 2017. Table 2-6 summarizes their design and as-built containment capacities.

Component	Western EDCB	Eastern EDCB
Permitted Design Capacity	120 m <sup>3</sup>	120 m <sup>3</sup>
Required Design Capacity	97 m <sup>3</sup>	85 m <sup>3</sup>
As-Built Design Capacity	124 m <sup>3</sup>	85 m <sup>3</sup>

#### Table 2-6. EDCB Design and As-built Capacities

## 2.3.8 Reclaim and TIA Water Discharge System

The TIA Reclaim and Roberts Bay Discharge System consist of high-density polyethylene (HDPE) pipelines, some of which are heat traced, and pumps sized to manage water in the TIA.

The Roberts Bay Discharge System was commissioned in February 2020 and historically was run intermittently as allowed by water quality to manage the water level in the Reclaim Pond. In 2023, a new effluent water treatment plant (EWTP) and reclaim pumphouse pad were constructed near the Reclaim Pond on a bedrock outcrop near the North Dam (Figure 2). The new EWTP provides additional water treatment capacity and allows for higher rates and extended discharge periods. Intake from the Reclaim Pond occurs via the intake line and reclaim pump house (710) which pumps water to the mill during operations via the new EWTP or bypassing the plant if used for reclaim water make-up and re-use in the mill. Since entering Care and Maintenance and the cessation of mill operation (October 2021), no reclaim water has been pumped to the mill.

The current reclaim pad is constructed at approximately 36.4 masl, above the maximum water level of the North Dam.

## 2.4 Tailings Impoundment Area Instrumentation

The Dam instrumentation is monitored and maintained in accordance with the North and South Dam Monitoring Standard Operating Procedure (SOP) (SRK 2022c and 2022d). The following sections detail the instrumentation by area.

## 2.4.1 North Dam

The active performance monitoring instrumentation for the North Dam consists of:

- Fifteen vertical ground temperature cables (GTCs);
- Thirteen horizontal GTCs;

- Eighteen surficial survey monitoring points located on the downstream face of the dam;
- Nine surficial survey monitoring points located on the upstream face;
- Fourteen crest survey monitoring points located along the upstream and downstream crest of the dam;
- Three deep settlement points;
- Six inclinometers located within the downstream face; and
- Twelve single bead thermistors, measuring thermosyphon contact temperatures.

The nine upstream surficial survey monitoring points were installed to monitor for expected deformation as the upstream foundation warms. Monitoring of these upstream points commenced in June 2023.

Figure 4 through Figure 6 show the location of North Dam instrumentation. All GTCs are connected to dataloggers allowing continuous data collection. Slope inclinometers are recorded manually using a slope inclinometer instrument owned by Agnico Eagle. Settlement monitoring is currently completed using RTK GPS, prior to the 2023 monitoring year, a total station was used.

#### 2.4.2 South Dam

The active South Dam performance monitoring instrumentation consists of:

- Nine horizontal GTCs;
  - one transverse GTC along the GCL interface at the upstream top crest of the key trench (SD-HTS-B1-KT);
- Fifteen vertical GTCs;
- Nineteen surficial survey monitoring points (crest and downstream slope);
- Thirteen crest survey monitoring points; and
- Three deep settlement points.

The monitoring instrument locations are shown in Figure 7 and Figure 9. Eleven active GTCs are connected to dataloggers allowing continuous data collection and transmission. The data are accessed from an online portal.

#### 2.4.3 West Dam

The West Dam is not yet constructed.

#### 2.4.4 Interim Dike

The Interim Dike is monitored using three ground temperature cables (GTC). Two GTCs are installed on the north side of the Interim Dike and one on the upstream side (south). Periodic topographic surveys are also collected in addition to visual monitoring.

Weekly visual inspections and temperature readings from these GTCs are ongoing and a formal monitoring program is being developed by Agnico Eagle. An updated monitoring SOP is expected to be a part of the next OMS update.

## 2.4.5 Other TIA Instrumentation and Monitoring

The monitoring of the water level in the Reclaim Pond is summarized below:

- The water level in the TIA Reclaim Pond is monitored by an automated pressure transducer and data logger installed at monitoring point TIA-2. The data are transmitted by a solar-powered iridium satellite transceiver to an online portal where they can be accessed remotely by Agnico Eagle and SRK. There is also a backup datalogger installed to record pond levels should a problem occur with the primary data collection system.
- The primary datalogger is configured to collect a reading every 15 minutes in the summer and every 60 minutes during the winter. The data is transmitted to the online portal every 5 days, and daily during the freshet season.
- On an annual basis, another consultant conducts a water level reference survey and as required a bathymetry survey of the TIA basin. Based on communications from Agnico Eagle, the water level constant elevation was adjusted from 27.761 masl (ERM 2017) to 27.71 m on August 15, 2019, at 00:00, this constant remained unchanged for 2024.

Other instrumentation includes:

- Tailings deposition volumes are monitored with a flowmeter and an automated data collection system;
- Reclaim water is measured using a flowmeter with an automated data collection system;
- Mine water discharge rates are measured by a totalizer instrument, recorded manually twice daily; and
- Comprehensive climate data from the Doris meteorological station is maintained in a database for review in conjunction with any TIA monitoring.

## 2.5 Dam Hazard Classification

Dam hazard classifications for the North Dam, South Dam and West Dam were conducted as part of the design and included in the approved final environmental impact statement (SRK 2017e). The classifications were done in accordance with the Canadian Dam Safety Guidelines (CDA 2013) (Table 2-7) as well as the CDA Technical Bulletin on Application of Dam Safety Guidelines to Mining Dams (CDA 2014). The classification was reviewed as part of the 2019 AGI (SRK 2020a) in conjunction with the updated CDA bulletin (2019), at the time no changes in the TIA operations or context warranted modification to the hazard rating of HIGH for the constructed North and South Dams. The designated dam hazard classifications assigned to each structure are listed in Table 2-8 (SRK 2015, 2016b, 2017e).

In line with recommendations from the 2021 DSR, a review of the dam hazard classification should be undertaken prior to resuming operations and reference the 2023 CDA Technical Bulletin on Environmental Consequence Classification.

	Population	Incremental losses			
Dam Class	at Risk <sup>1</sup>	Loss of Life <sup>2</sup>	Environmental and Cultural Values	Infrastructure and Economics	
Low	None	0	Minimal short-term loss No long-term loss	Low economic losses; area contains limited infrastructure or services.	
Significant	Temporary only	Unspecified	No significant loss or deterioration of fish or wildlife habitat Loss of marginal habitat only Restoration or compensation in kind highly possible	Losses to recreational facilities, seasonal workplaces, and infrequently used transportation routes.	
High	Permanent	10 or fewer	Significant loss or deterioration of <i>important</i> fish or wildlife habitat Restoration or compensation in kind highly possible	High economic losses affecting infrastructure, public transportation, and commercial facilities.	
Very high	Permanent	100 or fewer	Significant loss or deterioration of <i>critical</i> fish or wildlife habitat Restoration or compensation in kind possible but impractical	Very high economic losses affecting important infrastructure or services (e.g., highway, industrial facility, storage facilities for dangerous substances).	
Extreme	Permanent	More than 100	Major loss of <i>critical</i> fish or wildlife habitat Restoration or compensation in kind impossible	Extreme losses affecting critical infrastructure or services (e.g., hospital, major industrial complex, major storage facilities for dangerous substances).	

#### Table 2-7: Dam Hazard Classification (CDA 2013, 2014, 2019)

Notes:

<sup>1</sup> Definitions for population at risk:

None – There is no identifiable population at risk, so there is no possibility of loss of life other than through unforeseeable misadventure.

Temporary – People are only temporarily in the dam-breach inundation zone (e.g., seasonal cottage use, passing through on transportation routes, participating in recreational activities).

Permanent – The population at risk is ordinarily located in the dam-breach inundation zone (e.g., as permanent residents); three consequence classes (high, very high, extreme) are proposed to allow for more detailed estimates of potential loss of life (to assist in decision-making if the appropriate analysis is carried out).

<sup>2</sup> Implications for loss of life:

Unspecified – The appropriate level of safety required at a dam where people are temporarily at risk depends on the number of people, the exposure time, the nature of their activity, and other conditions. A higher class could be appropriate, depending on the requirements. However, the design flood requirement, for example, might not be higher if the temporary population is not likely to be present during the flood season.

Structure	Population at Risk (PAR)	Loss of Life	Environmental and Cultural Values	Infrastructure and Economics	Overall Hazard Classification
North Dam	SIGNIFICANT	SIGNIFICANT	HIGH	LOW	HIGH
South Dam	SIGNIFICANT	SIGNIFICANT	HIGH	LOW	HIGH
West Dam (Not constructed)	SIGNIFICANT	SIGNIFICANT	HIGH	LOW	HIGH

#### Table 2-8: Dam Hazard Classification of TIA Containment Structures

# 3 TIA Management System Review Findings

## 3.1 Tailings Operating, Maintenance and Surveillance Manual

Agnico Eagle has completed a significant update to OMS manual and Emergency Response Plan to align with the Agnico Eagle standards and reflect the corporate governance structure. Agnico Eagle and SRK conducted a detailed review of the trigger, action, response plans for inclusion in the OMS manual. The OMS manual was updated in March 2024, and is reviewed and/or updated annually by Agnico Eagle. The OMS manual integrates the dam monitoring SOPs, TARPs, Emergency Response Plan as well as any changes to the tailings management system under Agnico Eagle's corporate tailings management system. A detailed review of the OMS manual is not part of the Annual Geotechnical Inspection.

The roles and responsibilities for the TIA are listed in the OMS manual, however some key personnel have changed, an abbreviated list of key responsible parties as of September 2024 is provided below. Note, all parties are Agnico Eagle personnel unless otherwise stated.

Role	Personnel Title
Accountable Executive Officer	Michel Julien Vice-president Environment and Critical Infrastructure
Engineer of Record <sup>(1)</sup>	Thomas Lepine Advisor, Environmental Management
Mine General Manager	Marc-Olivier Vachon
Design Engineer	John Kurylo Principal Geotechnical Engineer – SRK Consulting
Site Geotechnical Engineer	Brennan Jay
Environment General Supervisor / Responsible Person	Guy Dufour (Transitioned to Cyryl Jenkins, as of February 2025)
Independent Review Board	Bill Horne Independent Reviewer – Geocryology Inc. Henri Sangam Independent Review Board – Geomino Inc.
Health and Safety General Supervisor	Morgan Hjorth

#### Table 3-1: Roles and Responsibilities

Sources: AEM, 2024

Notes: 1) The Engineer of Record role for the TIA transferred from John Kurylo (SRK) to Thomas Lepine on January 1, 2022.

SRK supports monitoring of the TIA, and all monitoring data for the TIA is submitted to SRK for review and data is hosted in a database and available for visualization and review online.

## **Recommendation:**

 Update the monitoring SOPs for the North and South Dam to reflect all current monitoring instrumentation and procedures.

- Update the OMS manual to include any of the changes/revisions not captured in the current version of the OMS, including the South Dam toe berm, Emergency Overflow Channel implementation timing and any changes because of the dam hazard classification review.
- OMS Manual, TARPs and Emergency Response Plan should be reviewed with the Agnico Eagle site operations annually, or after revisions; to ensure staff are appropriately informed and trained on the contents of these documents.

## 3.2 Independent Dam Safety Review and Risk Assessment

In accordance with CDA Dam Safety Guidelines (CDA 2013, 2014, 2019), including the CDA Technical Bulletin on Dam Safety Reviews (CDA 2016), independent third-party dam safety reviews (DSRs) should be conducted in accordance with a frequency informed by the hazard classification of the structures. It is recommended that HIGH hazard classification dams, such as the North Dam and South Dam, undergo a dam safety review every seven years.

A DSR for the North and South dams was completed in 2021 by Tetra Tech Inc. (Tetra Tech 2022), and the next DSR should be planned for 2028. The findings from the 2021 DSR recommendations are being addressed.

Independent Review Board Meetings were held in July 2024.

#### **Recommendations:**

- Continue to address recommendations from the DSR.
- In line with recommendations from the DSR, the dam hazard classification should be reviewed and updated prior to resuming operations, and the review should consider the 2023 CDA Technical Bulletin on Environmental Consequence Classification.

## **TIA Inspection and Monitoring Instrumentation** 4 **Findings**

#### **Compliance with Monitoring Frequency Requirements** 4.1

The North Dam and South Dam monitoring frequency requirements are outlined in the OMS manual (AEM 2024).

The monitoring frequency requirements and actual monitoring frequency for the 2024 monitoring year (October 1, 2023 to September 30, 2024) are summarized for North and South Dams in Table 4-1 and Table 4-2, respectively. As a formal monitoring program is under development for the Interim Dike, a monitoring frequency summary is provided without a conformance column.

Element	Item	Method	Responsibility	Required Frequency	Conformance with Frequency Requirements (AEM 2024) <sup>(1)(2)</sup>	Comments	
	Ground Temperature Cables	Datalogger		Daily (automated)	Yes	Recorded four times daily	
Thermal	Thermosyphons		Agnico Eagle	· · · · ·	Yes	Record four times daily	
	Datalogger downloads	Manual		Monthly	Yes	Data collected monthly	
Deformation	Downstream Surface Settlement				No	Four of seven monthly surveys received	
	Downstream Deep Settlement	Manual	Agnico Eagle	Monthly (May to Nov.)	No	with the survey equipment that have been addressed for 2025).	
	Crest Settlement				No		
	Depressions				Yes	No changes observed	
	Inclinometers			Monthly	Yes	Data collected monthly, except when inclinometer was off site for servicing	
	Water Level	Datalogger / Pressure Transducer		Daily (automated)	Yes	Readings every 15 min and uploaded daily during open water season, every 60 min and uploaded ever 5 days during winter.	
Water Balance	Water Level	Manual	Agnico Eagle	Monthly	Yes	Manual water level surveys only required if a datalogger is not in place, however monthly elevation checks are suggested in conjunction with the North Dam surveys. Water level constant for pressure transducer is checked annually during open water season.	
	Seepage Monitoring <sup>(5)</sup>			Monthly when flowing water is	Yes		

#### Table 4-1: North Dam Monitoring Frequency Requirements for the 2024 Monitoring Year<sup>(1)</sup>

Element	Item	Method	Responsibility	Required Frequency	Conformance with Frequency Requirements (AEM 2024) <sup>(1)(2)</sup>	Comments
Visual	Visual Walkover Inspection and Reporting	Visual	Agnico Eagle	Weekly (below FSL <sup>(3)</sup> ) Daily (at or above FSL)	Yes	Inspections conducted weekly, except when access was not available. <sup>(4)</sup>
	Annual Geotechnical Inspection	Inspection	Independent Qualified Licensed Geotechnical Engineer	Annually	Yes	September 2024 (This report)
Maintenance						
North Dam Thermal	Datalogger Primary Batteries	Manually recharge		Annually (Or as needed)	No	Recharged December 2022
	Datalogger Backup Batteries	Manually replace		5-year cycle	Yes	Replaced during datalogger recalibration
Datalogger	Datalogger Recalibration	Manual	A main a Franka		Yes	Completed Jan. 2018
	Desiccant Packs	Manually replace	Agnico Eagle	As required	Not required	Replace moisture indicators in 2025.
Water Level Datalogger Station (TIA-2)	Datalogger Transmission Subscription	Online		Annually	Yes	15% of the data subscription remains (as of December 20, 2024)
	Physical Datalogger Station	Manually recalibrate or replace		As required	Not required	No action required

#### Note(s):

<sup>1</sup> The monitoring year (or data reporting period) included in this report was October 1, 2023 to September 30, 2024.

<sup>2</sup> This column lists if the monitoring frequency is compliant with the monitoring frequency requirements during this monitoring year.

<sup>3</sup> NOWL: Normal Operating Water Level (Previously referred to as Full Supply Level)

<sup>4</sup> Occasional inspections missed where dam access was not possible due to winter weather, road conditions or other operational constraints.

<sup>5</sup> The Seepage Monitoring standard operating procedure monitors the flowing water at the toe of the North Dam for chemical signature of seepage originating in the TIA Reclaim Pond, no chemical signature has been observed to date. The Seepage Monitoring SOP also includes TL-5 geochemical sampling and Geochemical QA/QA monthly while water flow is observed at the North Dam toe.

Element	ltem	Method	Resp.	Required Frequency	Conformance with Frequency Requirements (AEM 2024) <sup>(1)(2)</sup>	Comments	
Thermal	Ground Temperature Cables	Datalogger	Agnico Eagle	Daily (automated)	Yes	Data is transmitted every 12 hours. Some dataloggers have stopped transmitting data and AEM have attempted repair and replacement. Some transmission issues remain.	
	Deep Settlement				No	Four of seven monthly surveys received	
	Crest Settlement			Monthly	No	(Missed surveys were due to issues	
Deformation	Surficial Settlement	Manual	Agnico Eagle	(May – Nov.)	No	been addressed for 2025).	
	Depressions				Yes	No issues observed	
	Water Level	Datalogger	Agnico Eagle	Daily	Yes	Refer to Table 4-1	
Water Balance	Seepage Monitoring	Manual	Agnico Eagle	Weekly when observed (flowing water)	Yes	No flowing water observed.	
	Downstream Ponded Water	Manual	Agnico Eagle	Monthly when observed	Yes		
Visual	Visual Walkover Inspection		Agnico Eagle	Weekly (below NOWL <sup>(3)</sup> ) Daily (above NOWL)	Yes	Inspections conducted weekly, except when access was not available. <sup>(4)</sup>	
	Annual Geotechnical Inspection	Manual	Independent Qualified Licensed Geotechnical Engineer	Annually	Yes	September 2024 (This report)	
Maintenance							
	Datalogger Batteries	Solar recharge				Service or replace dataloggers or batteries that do not appear to	
South Dam	Datalogger Recalibration	Manual	Agnico Eagle	As needed	Yes	recharge in the summer via the photovoltaic cell.	
Thermal Datalogger	Desiccant Packs	Manual				Some dataloggers have stopped transmitting and require maintenance	

#### Table 4-2: South Dam Monitoring Frequency Requirements for the 2024 Monitoring Year <sup>(1)</sup>

Note(s):

<sup>1</sup> The monitoring year (or data reporting period) included in this report was October 1, 2023 to September 30, 2024.

<sup>2</sup> This column lists if the monitoring frequency is compliant with the monitoring frequency requirements during this monitoring year.

SRK/Agnico

Eagle

<sup>3</sup> NOWL: Normal Operating Water Level (Previously referred to as Full Supply Level)

Online

Datalogger

transmission

subscription

<sup>4</sup> Occasional inspections missed where dam access was not possible due to winter weather, road conditions or other operational constraints.

Annually

Yes

None

#### Table 4-3: Interim Dike Monitoring

Element	ltem	Method	Resp.	Required Frequency <sup>(1)</sup>	Comments
Thermal	Ground Temperature Cables	Datalogger	Agnico Eagle	Weekly (May to Nov) Monthly (December to April) Or Daily (if connected to datalogger)	Spot readings and periodic data logger readings. These GTCs should be connected to dataloggers.
Deformation	Topographic Survey	Survey	Agnico Eagle	Every two months – starting in May and continuing until snow covers the structure.	Topographic surveys of the Interim Dike should be completed once after snowmelt and once prior to freeze up (ideally every two months). Survey monitoring points should be established to allow monthly monitoring.
Water Balance	Upstream Water Level (Saline Water Pond)	Survey	Agnico Eagle	Monthly (ice free months)	Frequency may be increased at the discretion of the Site Geotechnical Engineer and/or EoR
	Visual Walkover Inspection		Agnico Eagle	Weekly (May to Nov) Monthly (December to April)	Inspections conducted weekly, except when access was not available. <sup>(2)</sup>
Visual	Annual Geotechnical Inspection	Manual	Independent Qualified Licensed Geotechnical Engineer	Annually	September 2024 (This report)

Note(s):

<sup>1</sup> As listed in the OMS Manual (AEM 2024)

<sup>2</sup> Occasional inspections missed where dike access was not possible due to winter weather, road conditions or other operational constraints.

#### **Recommendations:**

- Recommended monitoring frequencies have been met in most categories, however:
  - Three survey monitoring events we missed due to issues with the survey equipment (these have been addressed for 2025).
  - Some of the newly installed ground temperature cables on the North and South Dam are read infrequently and existing dataloggers have stopped transmitting. AEM have attempted repair and replacement. Some transmission issues remain.
  - AEM should aim to improve the frequency of the monitoring in 2025.
- Formalize and implement the monitoring program for the Interim Dike.
- Update the OMS manual and monitoring SOPs to include any new or updated instrumentation.

## 4.2 North Dam Inspection and Monitoring

## 4.2.1 Overall (Visual) Inspection of the North Dam during the AGI

As part of the 2024 AGI a visual inspection of the North Dam was completed. At the time of the inspection, the North Dam appeared to be in good condition, and no issues of concern were observed. Observations and recommendations related to instrumentation and monitoring points are provided in the following sections.

Cracking has been previously noted on the GTC datalogger housings. These cracks are located on the flange that connects the housing to the riser and the cracks do not appear to penetrate through the housing. The interior of the housings were dry and no evidence of moisture ingress was noted during the inspection. A thorough inspection should be conducted each spring for signs of moisture ingress, and repairs conducted where moisture ingress is observed. Consider replacement of all moisture indicators, and desiccant packets as needed.

Minor depressions in the rock fill have been observed periodically since construction on both the upstream and downstream sides. On the upstream side of the dam, particularly below the high-water line, ice and wave action is suspected to have caused movement of some of the ROQ rock and it is possible that localized thaw settlement has caused some increased undulation in the ROQ surface. These areas will be monitored for further changes, however at the time of inspection there was no cause for concern.

Tundra die-back was observed along the eastern upstream toe of the dam, below the high water mark. This area should be monitored closely over the next year for signs of thermal erosion and increased thaw settlement.

The attached Photolog (Photolog 1 to 3) provides a general overview of conditions on the North Dam.

#### **Recommendations:**

- Disturbance (track marking) on the tundra above the west abutment, due to drilling access during the EOC drilling investigation was previously noted (SRK, 2023b). This area was inspected in 2024 and no signs of erosion or permafrost degradation were observed in 2024, however the areas should continue to be monitored periodically and mitigation measures implemented if changes are observed.
- Tundra dieback observed along the upstream toe (below 33.05 masl, the maximum Reclaim Pond level) should include monitoring for erosion or increased permafrost thaw settlement in the future.
- Cover the dam face GTCs with non-woven geotextile and a thin layer of rock for protection and to improve the quality of the temperature readings.

## 4.2.2 Ground Temperature Cables

To monitor long-term temperature of the frozen core and the dam foundation, a total of twenty-four GTCs were installed during the North Dam construction (SRK 2012b). Of the twenty-four installed GTCs, twenty-two are still functional. Since September 2012, GTC data for the North Dam is recorded by two Campbell Scientific CR1000 dataloggers, and the data is downloaded directly from the dataloggers by Agnico Eagle personnel.

The data is recorded every six hours, unless otherwise noted, details on the status of the North Dam GTCs is summarized in Table 4-4, and a summary of the GTC measurements is provided in Table 4-5. The GTC data collection had no concerns in 2024.

Four additional vertical GTCs were installed in the upstream face of dam in February 2024, to monitor the thermal performance of the rockfill shell. Data is collected by manual spot readings or by automated data loggers.

GTC ID	Status	Comments				
ND-VTS-040-KT	Active	Disconnected for recalibration between January 1 to March 3, 2018				
ND-HTS-040-31.5	Active	Disconnected for recalibration between January 1 to March 3, 2018				
		Cable disconnected from datalogger October 10, 2013 to May 12, 2014				
ND-HTS-040-33.5	Active	Connection to datalogger more permanently repaired July 2014				
		Disconnected for recalibration between January 1 to March 3, 2018				
ND-VTS-060-US	Inactive	Irreparably damaged between April 27 and August 8, 2012				
ND-VTS-060-USS1	Active	Installed February 2024. Spot readings collected periodically through 2024.				
ND-VTS-060-DS	Active	Disconnected for recalibration between January 1 to March 3, 2018				
ND-VTS-060-KT	Active	Spliced during construction. Fully operational, except for recalibration January 1 to March 3, 2018				
		Bead 7 – Works intermittently, and since fall 2016 has occasional erratic readings that are attributed to instrumentation errors.				
ND-HTS-060-28.8	Active	ead 9 – Works intermittently				
		Disconnected for recalibration between January 1 to March 3, 2018				
ND-HTS-060-31.0	Active	Disconnected for recalibration between January 1 to March 3, 2018				
ND-HTS-060-33.5	Active	Disconnected for recalibration between January 1 to March 3, 2018				
	Active	Erratic data at most beads (excluding Beads 3, 6 and 9) between June 2016 and May 2017 with lower amplitude spikes between December 2016 and May 2017.				
ND-VTS-085-US		Erratic data subsided since May 2017				
		Disconnected for recalibration between January 1 to March 3, 2018				
ND-VTS-085-USS1	Active	Installed February 2024, spot readings began in March 2024 and continuous datalogger readings began in August 2024.				
ND-VTS-085-USS2	Active	Installed February 2024, spot readings began in March 2024 and continuous datalogger readings began in August 2024.				
ND-HTS-085-US	Active	Installed on the upstream face of the dam. Readings collected July to October 2024.				
ND-VTS-085-DS	Active	Erratic data at most beads (excluding Beads 3, 6 and 9) between June 2016 and May 2017 with lower amplitude spikes between December 2016 and May 2017. Erratic readings have not been recorded since May 2017.				
		Disconnected for recalibration between January 1 to March 3, 2018				
ND-VTS-085-KT	Active	Erratic data at most beads (excluding Beads 3, 6 and 9) between June 2016 and May 2017 with lower amplitude spikes between December 2016 and May 2017. Erratic readings have not been recorded since May 2017.				
		Disconnected for recalibration between January 1 to March 3, 2018				
ND-HTS-085-25.3	Active	Disconnected for recalibration between January 1 to March 3, 2018				
ND-HTS-085-29.4	Active	Disconnected for recalibration between January 1 to March 3, 2018				
ND-HTS-085-33.5	Inactive	Irreparably damaged during construction				

Table 4-4: North Dam Ground Temperature Cable Status

GTC ID	Status	Comments
		Bead 9 – Periods of erratic readings since June 2016 (temperature dropping randomly to less than -15°C)
		Disconnected for recalibration between January 1 to March 3, 2018
ND-VTS-130-US	Active	Bead 1- Offline since August 13, 2020 and August 18, 2023
		Bead 8 - Offline from February 25 to September 21, 2021 and November 4, 2021 to August 11, 2022
		Bead 10 – Erratic readings for periods since May 2022
ND-VTS-130-USS1	Active	Installed February 2024. Spot readings collected periodically through 2024.
		Small magnitude temperature spikes during summer months between 2013 and 2017 (Bead 3, 7, 8, 9, 11), no spikes observed in 2018 through 2021, spikes were observed in 2022 and 2023.
ND-VTS-130-DS	Active	Beads 3 – 8 were offline after the connector at the datalogger housing was damaged on September 24, 2017. Repaired and reconnected on March 11, 2018 following datalogger recalibration
		Disconnected for recalibration between January 1 to March 3, 2018. Beads 3 to 8 were disconnected and repaired between September 24, 2017 and March 3, 2018 (due to damaged cable connection)
ND-VTS-130-KT	Active	Disconnected for recalibration between January 1 to March 3, 2018
		All beads were offline after the connector at the datalogger housing was damaged on September 24, 2017. Repaired and reconnected on March 4, 2018 following datalogger recalibration
ND-HTS-130-28.8	Active	Disconnected for recalibration between January 1 to March 3, 2018
		Bead 2 – Erratic readings and intermittent logging in Summer 2018, 2019 and 2020
ND-HTS-130-31.0	Active	Disconnected for recalibration between January 1 to March 3, 2018
ND-HTS-130-33.5	Active	Fully operational, except for cable repair and recalibration between September 24, 2017 and March 3, 2018
		Spliced during construction
ND-VTS-175-KT	Active	Incorrectly connected to datalogger as ND-HTS-175-33.5 from August 9, 2012 to June 16, 2014, therefore Beads 9, 10 and 11 had no readings during this time.
		Disconnected for recalibration between January 1 to March 3, 2018
ND-HTS-175-32.5	Active	Disconnected for recalibration between January 1 to March 3, 2018
		Spliced during construction
ND-HTS-175-33.5	Active	Incorrectly connected to datalogger as ND-HTS-175-KT, from August 9, 2012 to June 16, 2014
		Disconnected for recalibration between January 1 to March 3, 2018

Zone	Horizontal GTCs (Core)	Vertical GTCs (KT)	Observation
Design Temperature	−2°C	-8°C	The minimum criteria required to ensure Dam is performing in accordance with design specifications (normal operating conditions)
Station 0+040	Meets	Meets	Temperatures are below the design specification with substantive safety buffer. Slight warming trend observed but appears to be counteracted by the active cooling of the thermosyphons. An active thermosyphon cooling system was implemented in July 2024 (Section 4.2.3), resulting in improved thermal performance in this zone of the dam. All temperatures are below the maximum temperature criteria.
Station 0+060	Meets	Meets	Temperatures are below the design specification with substantive safety buffer within the central core (Critical Zone) Upstream most beads indicate a recent warming trend, observed beginning in 2023, related to rising water levels in the reclaim pond combined with a warmer winter 2024. All temperatures in the core remain below -2°C. An active thermosyphon cooling system was implemented in July 2024 (Section 4.2.3), resulting in improved thermal performance in this zone of the dam. These GTCs are being closely monitored by AFM and SRK
Station 0+085	Meets (Upstream- most bead exceeded -2°C)	Meets	Temperatures are below the design specification with substantive safety buffer within the central core (Critical Zone). Upstream most beads within the core indicate rising temperatures beginning in 2019 and becoming more notable in 2022 to 2024. The upstream most beads within the core (ND-HTS-085-25.3 and ND-HTS-085-29.4) exceeded -2°C between August 2023 and May 2024, and peaked at -1.71 °C (December 2023) and has since cooled to below -2 °C. The warming trend is related to rising water levels in the reclaim pond combined with a warmer Q3 2023 and Q1 2024. All other temperatures in the core remain below -2°C. An active thermosyphon cooling system was implemented in July 2024 (Section 4.2.3), resulting in improved thermal performance in this zone of the dam . These GTCs are being closely monitored by AEM and SRK.
Station 0+130	Meets	Meets	Temperatures are below the design specification with substantive safety buffer within the central core (Critical Zone). Upstream most beads indicate a recent warming trend, observed beginning in 2023, related to rising water levels in the reclaim pond combined with a warmer winter 2024. All temperatures in the core remain below -2°C. An active thermosyphon cooling system was implemented in July 2024 (Section 4.2.3), resulting in improved thermal performance in this zone of the dam. These GTCs are being closely monitored by AEM and SRK.

#### Table 4-5: Summary of Core and Key Trench Ground Temperature Cable Observations

Zone	Horizontal GTCs (Core)	Vertical GTCs (KT)	Observation
Station 0+175	Meets	Meets	Generally performing as expected with substantive safety buffer and stable trend in the core, and slight cooling trend in the foundation An active thermosyphon cooling system was implemented in July 2024 (Section 4.2.3), resulting in improved thermal performance in this zone of the dam

Since the accelerated warming trend was observed in September 2023 (Table 4-5), AEM has changed the TARP level to Yellow (level 1) and subsequently to Orange (level 2) in April 2024. The TARP level change has resulted in increased frequency of GTC monitoring to every two weeks, data review, meetings with the internal review board members and thermal modelling have been ongoing since the observations. Following the TARP change to Orange, additional mitigation measures including reducing the water level on the upstream side (to reduce thermal loading) and implementation of an active cooling system on the passive thermosyphons (July 2024). Additional engineering mitigations are being considered to maintain performance of the North Dam.

The data collected to the end of December 2024 (not shown in Appendices) indicate core temperatures have continued to decrease as the thermosyphons become operational and the surface boundary cools with the air temperature. The GTCs will continue to be closely monitored in support of the additional review meetings and thermal modelling which are ongoing.

## **Recommendations:**

- Continue to closely monitor warming conditions along upstream side of the North Dam and continue to monitor the results, adhere to the TARPs, plan/implement additional review meetings, analysis and implement responses/mitigations accordingly.
- Continue downloading data every two weeks until observed warming conditions subside.
- Consider implementing dataloggers for all new GTCs, and continue manual spot readings until dataloggers are installed.
- Cover the dam face GTCs with non-woven geotextile and a thin layer of rock for protection and to improve the quality of the temperature readings.

## 4.2.3 Thermosyphons

Thermosyphon temperature monitoring for the North Dam has been automated. Single bead thermistors connected to the datalogger system are attached to each thermosyphon evaporator pipe below the ground surface, and insulation has been placed around the thermistor beads to ensure the evaporator pipe temperature, and not the ambient air temperature, is measured (SRK 2012b). Additionally, air temperatures are recorded at the dataloggers every six hours. This data are downloaded as part of the monthly ground temperature cable datalogger downloads.

To monitor the performance of the thermosyphons, thermosyphon evaporator pipe contact temperatures and air temperatures are plotted against time.

During the winter months, when the thermosyphons are operating passively, the thermosyphon pipe temperatures are typically 5°C warmer than the air temperature. If the thermosyphon pipe temperature during the winter months is approximately the same as the air temperature, it indicates that the thermosyphon is not working correctly. Thermistor data indicates all the south and north thermosyphons are functioning except for North 2 (Appendix B).

As documented in past AGI's (SRK 2023) Since 2012, the measured pipe temperature of North 2 was only slightly higher than the measured air temperature, which indicates a malfunction. Ground temperature readings near the North 2 thermosyphon pipe support the conclusion that the North 2 thermosyphon is not working correctly. Efforts to investigate and remediate the non-functional thermosyphon through practical measures have been exhausted, including a detailed inspection during installation of the active cooling system. Thermal modelling of the frozen core has considered loss of the North 2 thermosyphon. Any additional measures will be taken as necessary based on the observed performance of the overall dam.

The hybrid thermosyphon active refrigeration has effectively reduced the peak temperatures in 2024 and are expected to continue to remove heat from the foundation in subsequent years. The south bank of thermosyphons are operational since July 11, 2024. The north bank active cooling system was operational from July 11 to September 20, 2024 however stopped operating due to issues with the refrigeration unit. Passive cooling resumed in November 2024.

Arctic Foundations is planned to be on site in 2025 to troubleshoot the south refrigeration unit in 2025, in order to resume active cooling once the passive cooling stops at the end of winter 2025.

#### **Recommendations:**

- Troubleshoot and repair the active refrigeration system prior to the end of the passive thermosyphon cooling period (Typically ending in April).
- Update the OMS to include considerations for the operations, maintenance and monitoring of the hybrid thermosyphon cooling system.
- After at least one full season of operation, review the performance of the active cooling system and assess the effectiveness of the system.

## 4.2.4 GTC Datalogger Battery Voltage

Each CR1000 datalogger is powered by an external lead acid battery. Battery voltage is an important indicator of datalogger performance. If the battery voltage drops below 12 V, it is operating outside of the optimal range. At or below 9.6 V, voltage is outside of the operating range and the recorded readings could be incorrect, or the datalogger will shut down and readings would not be recorded.

The dataloggers record the minimum battery voltage four times daily. A graph of battery voltage versus time is provided in Appendix C.

#### **Recommendations:**

Recharge the CR-1000 Batteries as the voltage of CR-1000#2 Battery is below 12.0V

#### 4.2.5 Inclinometers

Six inclinometers were installed within the downstream face of the North Dam at the time of construction (2012). These inclinometers are used along with the survey monitoring points to monitor deformation within the dam and dam foundation. Inclinometer readings are taken by Agnico Eagle site personnel.

Inclinometer measurements are provided in Appendix D, and the data quality for the surveys has been good.

The inclinometer profiles show only negligible displacements in the dam foundation, and small displacements over the portion of the inclinometer above the natural ground surface as summarized in Table 4-6. Inclinometer ND-IN-120-3 is the only inclinometer that suggests a trend of downslope movement, with a maximum total magnitude is 5.3 cm since installation in 2012. All other inclinometers are showing minimal movement, or the movement is oscillating seasonally which likely indicates there is some movement of the inclinometer casing itself, as opposed to actual deformation of the dam or foundation.

	Maximum Overall Deformation		Maximum	Foundation De (m)		
Inclinometer	Magnitude (m)	Depth Below Dam Shell (m)	Magnitude (m)	Depth To Foundation (m)	Depth Below Dam Shell (m)	Observations
ND-IN-070-1	0.028	1.0	Less than 0.005	9.5	9.5 – 15.0	Minor deformation trend since 2015
ND-IN-070-2	0.036	1.5	0.016	9.0	9.0	Seasonal oscillation.
ND-IN-070-3	0.017	1.5	Less than 0.005	7.5	7.5 – 13.0	Minor deformation trend since 2015
ND-IN-120-1	0.012	0	Less than 0.005	7.0	7.0 – 12.0	Minor deformation trend upstream, constant since May 2016
ND-IN-120-2	0.022	0	Less than 0.005	6.0	6.0 – 11.0	Displacement trend constant since November 2017.
ND-IN-120-3	0.053	0	Less than 0.005	3.7	3.7 – 4.5	General trend of movement in dam shell, towards the northwest. The rate has increased slightly since 2021 (7mm/yr).

# Table 4-6: Summary of Inclinometer Measurement Observations (Sep. 2012 through September 2024)

The inclinometer was sent to Durham-Geo Slope Indicator (DGSI) for service and recalibration in 2023. The next service and recalibration should be planned for 2026.

During the inspection in 2023, it was noted that the inclinometer grooves were not exactly oriented in perpendicular-to-crest and parallel-to-crest orientations. During the 2024 inspection, the inclinometer casing orientations were measured relative to the dam crest, going forward inclinometer casing orientations should be recorded once per year to determine if the casings are rotating.

#### **Recommendations:**

- Record the inclinometer casing groove directions annually for at least three years to verify if there
  is any ongoing rotation. Take groove direction readings relative to the line of inclinometer casings
  (perpendicular to crest).
- Consider installation of automated inclinometer readings, via in place inclinometer (IPI) or shape accel array (SAA) to improve precision, continuity and reduce gaps associated with long inclinometer probe repair periods.

## 4.2.6 Survey Monitoring Points

The OMS (AEM 2024) outlines that survey data should be collected monthly between May and November. Survey monitoring of the North Dam occurred four times during the monitoring year, two less than recommended, due to issues with the GPS survey equipment.

Since construction, deep settlement and crest displacement have been small and of similar magnitude. Displacement, of these monitoring points, has essentially been unchanged since September 2013, confirming that much of the measured displacement to date is all directly related to the period immediately following construction. Complete survey data is presented in Appendix E.

Since 2013, the magnitude of displacement in the downstream dam shell has been minimal overall. There has been a persistent trend of horizontal displacement at ND-SSP-155-2 and ND-SSP-110-3, both situated near the downstream toe, starting from June 2016 and continuing into 2024. The vertical displacement at these points has been limited. This increased horizontal movement is likely due to the gradual thawing of the active layer beneath the shallow rockfill at the toe of the dam and the lateral displacement or rotation of the monitoring point boulder where the survey pin is installed. ND-DSP-070 has indicated a vertical displacement in the last survey of 2024 and will continue to be monitored for a credible displacement trend. The survey data do not indicate any immediate concerns and visual inspection of the dam shell do not identify any notable signs of displacement.

Monitoring of the upstream survey monuments began on June 11, 2023. The data indicate an increasing trend in displacement for ND-SSP-125-US-2, reaching a maximum total displacement of approximately 0.3 meters in August 2024. This is likely influenced by deformations associated with historically high-water level.

No data has been received since October 14, 2023 for SSP-065-US-2, SSP-085-US-1, SSP-100-US-1 and SSP-160-US-1. These points were damaged due to snow clearing during installation of the upstream GTCs and should be re-established.

#### **Recommendations:**

- Integrate new upstream surficial survey points into the North Dam monitoring SOP and OMS.
- Re-establish the surficial survey points that were damaged due to snow removal and install flags to prevent future damage when heavy equipment is working nearby.

## 4.2.7 Visual Inspection

Visual inspections of the North Dam are required weekly when the TIA water level is below the full supply level. All weekly visual inspection reports, including photos, are maintained by AEM on an internal system and are not provided in the AGI. The visual inspections report and track changes to the dam surface, visible damage to instrumentation, signs of erosion or seepage, or any other surface anomalies.

#### **Recommendations:**

No recommendations

#### 4.2.8 Monitoring of Water at the Toe of the North Dam

The monitoring of the flowing water at the North Dam toe is described in the Monitoring SOP and OMS Manual (AEM 2024). The intent of this monitoring is to verify that there is no chemical signature of the Reclaim Pond in the water emanating from the toe of the dam (hypothesized to be percolation of precipitation and snowmelt from the ROQ dam shell voids. The program includes routine water quality sampling. SRK's review of the 2024 water quality is ongoing and reported separately.

#### **Recommendations:**

- No change to recommendations
- The v-notch weir at the toe of the dam does not provide accurate flow measurements. Consider decommissioning if disturbance to the toe of the dam can be minimized, or it may be left in place provided no signs of thermal degradation at the toe are observed.
- If a change in typical water flow rates is observed (subjective) this should be noted on the visual inspection form.

## 4.3 South Dam Inspection and Monitoring

## 4.3.1 Overall (Visual) Inspection of the South Dam During the AGI

As part of the AGI, a visual inspection of the South Dam was completed. Overall, the dam is performing as expected and there were no significant issues noted. Observations and recommendations related to monitoring instrumentation are provided in the following sections.
The construction of the South Dam toe berm has addressed the cracking due to relaxation of the downstream slope of the dam, within the section of the dam retaining the Phase 1 tailings beach. Tension cracks of different length and aperture are visible at the toe berm, with limited change from 2023. No new tension cracks were observed on the downstream slope of the dam, indicating the downstream berm is functioning as intended. Tension cracking is still visible along the abutments constructed to support the Phase 2 dam raise. Cracking in the Phase 2 abutment areas does not impact the performance of the Phase 1 tailings retaining portion of the dam; however, it does pose a potential maintenance issue and could require future mitigation if the cracking were to propagate more than currently observed. The most prominent tension crack is located on the southeastern side of the downstream rock shell (abutment) along the steeper slope and is attributed to active layer thaw settlement.

Ponded water has been observed at the downstream toe of the dam since construction and was observed to contain frost wedge polygons and standing water prior to construction. In past years the pond size was observed to be larger, however in 2024 the pond appears to have decreased in size and is not a cause for concern.

Both the downstream ponding and cracking are within the ultimate Phase 2 footprint and will be covered by the South Dam raise, so any additional proactive mitigation should be considered with this in mind.

Additionally, some minor ponded areas are noted on the tailings beach near the upstream shell, which appears to be precipitation runoff ponded in minor localized depressions.

There has been a notable increase in tailings dust on the dam shell since 2023. Site observations suggest that conditions have improved compared to earlier in the year, with the most dust being visible following freshet. Along the downstream toe, small amounts of tailings were visible on vegetation (i.e. a dust coating). Past visual inspections (Section 4.3.4) have noted small amounts of tailings on the melting snow drifts early in the summer. It is hypothesized that this has been transported during periods of strong winds from the north. Visual, dust, water quality monitoring is ongoing. Flooding of the Saline Pond (retained by the Interim Dike) may have a positive impact on reducing dust generation however this should be considered with the integrity of the structure in mind. Dust mitigation on the southern extents of the beach should be considered if the remaining upland beach is expected to remain dry for multiple years. At the time of inspection, the wind transported tailings visible on the ground was only observed on or immediately downstream South Dam toe (within five meters). AEM should continue their tailing dust related monitoring program and consider adding dust fall monitoring or similar.

On the tailings beach, tailings borrow areas were created during the construction of the Interim Dike. This borrow area is now partially flooded by the Saline Pond, and the Saline Pond is closer to the South Dam than previously observed due to this excavation. However, the Saline Pond, is still outside the recommended 100-meter buffer from the South Dam. Additional tailings excavation or farming should be avoided within 100-meters of the South Dam to maintain the required beach lengths.

Photolog 4 to 6 provide a general overview of the South Dam conditions at the time of the AGI.

#### **Recommendations:**

- The Phase 2 abutment tension cracks (outside of the lateral Phase 1 tailings extent) should continue to be monitored and plans to mitigate this if the cracking progresses to the point where progressive thaw slumps could be expected.
- Continue the tailing dust related monitoring program and consider adding dust fall monitoring as appropriate.
- Dust mitigation on the southern extents of the beach should be considered until deposition is planned to be resumed.
- Avoid tailings excavation or farming within 100 m of South Dam to maintain beach lengths.

### 4.3.2 Ground Temperature Cables and Dataloggers

To monitor long-term thermal performance of the frozen foundation dam, a total of twenty-seven GTCs were installed during South Dam construction (SRK 2018c) and four new cables were installed in November 2023. Three of the new cable were installed to replace cables damaged during construction, and one was installed in the tailings beach upstream of the dam. The original GTCs are connected to Beaded Stream Dataloggers (D505) to allow continuous data capture, and spot readings have been collected to-date for the new GTC. Table 4-7 provides a summary of the GTC status during the monitoring year.

GTC ID	Station ID	Status	# of Sensors (Functional / As-built)	Cable Serial Number		Comment
SD-VTS-065-KT	0+65	Active	11 / 11	3259	•	Offline for short periods in previous years (Appendix A)
SD-HTS-065-US	0+65	Inactive (2024)	5/5	3263	•	Offline for short periods in previous years (Appendix A) Currently offline – last data available on July 19, 2024
SD-HTS-155-US	1+55	Inactive (2024)	5/5	3266	•	Currently offline – Last data available on July 19, 2024
SD-HTS-155-KT	1+55	Inactive	0 / 11	-	•	Damaged during construction (irreparable)
SD-VTS-155-KT	1+55	Active	11 / 11	3251	•	Offline for short periods in previous years (Appendix A)
SD-VTS-155-US	1+55	Inactive	0 / 11	3272	•	Single sensor functioning until November 9, 2019

#### Table 4-7: South Dam Ground Temperature Cable Status Summary

GTC ID	Station ID	Status	# of Sensors (Functional / As-built)	Cable Serial Number		Comment
					•	No data since November 2019 (irreparable damage)
SD-VTS-155-DS	1+55	Inactive (2024)	11 / 11	3264	•	Currently offline – Last data available on July 19, 2024
SD-HTS-240-KT	2+40	Active	11 / 11	3254	:	Offline for short periods in previous years (Appendix A) Data gaps between January 23, 2024 and March
SD-HTS-240-US	2+40	Inactive (2024)	7/7	3269	:	Offline for short periods in previous years (Appendix A) Currently offline – Last data available on Aug 3, 2024. Suspected datalogger issue (unresolved).
SD-VTS-240-KT	2+40	Inactive (2024)	11 / 11	3255	•	Offline for short periods in previous years (Appendix A) Currently offline – Last data available November 12, 2023, Suspected cable may have been disconnected or damaged during installation of new upstream cables.
SD-VTS-240-US	2+40	Inactive (Replaced)	0 / 11	3268	•	Measurements ended on October 10, 2019 Replacement cable (SD-VTS-240-US1) installed November 2023
SD-VTS-240- US1	2+40	Active	11/11	4454	•	Installed November 2023, periodic spot readings through 2024 (See Appendix A)
SD-VTS-240-DS	2+40	Inactive (Replaced)	0 / 11	3265	•	Measurements ended on October 22, 2019 (irreparable damage) Replacement cable (SD-VTS-240-DS1) installed November 2023
SD-VTS-240- DS1	2+40	Active	11/11	4453	•	Installed November 2023, periodic spot readings through 2024 (See Appendix A)
SD-HTS-365-KT	3+65	Active	11 / 11	3257	•	Offline for short periods in previous years (Appendix A) No data between December 2, 2023 and March 18, 2024 due to datalogger troubleshooting

GTC ID	Station ID	Status	# of Sensors (Functional / As-built)	Cable Serial Number		Comment
SD-HTS-365-US	3+65	Active	11 / 11	3271	•	Continuously operational since construction
SD-VTS-365-KT	3+65	Inactive	0 / 11	-	•	Damaged following construction (irreparable)
						Bead 2 inactive
SD-VTS-365-US	3+65	Active	10 / 11	3270	•	Offline for short periods in previous years (Appendix A)
						No data collected from December 2, 2023 and March 18, 2024 due to datalogger troubleshooting
	Inostin				•	Measurements ended on August 3, 2020 (Irreparable damage)
SD-VIS-365-DS	3+65	(Replaced)	0 / 11	3275	•	Replacement cable (SD-VTS-360-DS) installed November 2023
SD-VTS-360-DS	3+65	Active	11/11	4456	•	Installed November 2023, periodic spot readings through 2024 (See Appendix A)
					•	Installed in suspected ground ice wedge near upstream toe
					•	Only bead 1 and 2 active
SD-VTS-US1	3+65	Active	2 / 13	3197	•	Offline for short periods in previous years (Appendix A)
					•	No data between December 2, 2023 and March 18, 2024 due to datalogger troubleshooting
					•	Installed in suspected ground ice wedge near upstream toe
					•	Only bead 1 active
SD-VTS-US2	3+65	Active	1 / 15	3189	•	Offline for short periods in previous years (Appendix A)
					•	No data between December 2, 2023 and March 18, 2024 due to datalogger troubleshooting
						Cable installed November 2023
SD-VTS-US3	3+65	Inactive	0/12	3194	•	Readings manually collected between November 14, 2023 and January 8, 2024. Cable unable to be read after January 8, 2024.

GTC ID	Station ID	Status	# of Sensors (Functional / As-built)	Cable Serial Number	Comment	
SD-HTS-460-KT	4+60	Inactive (2024)	11 / 11	3256	<ul> <li>Offline for short periods in previous years (Appendix A)</li> <li>Currently offline – Last data available on July 2024</li> </ul>	19,
SD-HTS-460-US	4+60	Inactive	0/5	-	<ul> <li>Damaged following construction (irreparable)</li> </ul>	
SD-VTS-460-KT	4+60	Active	11/11	3252	<ul> <li>Currently offline – Last data available on July 2024 (no prior issues). Suspected datalogger transmission issue.</li> </ul>	19,
SD-VTS-460-US	4+60	Active	11/11	3273	<ul> <li>Damaged following construction (repaired)</li> <li>Currently offline – Last data available on July 2024. Suspected datalogger transmission issued</li> </ul>	19, Je.
SD-VTS-460-DS	4+60	Inactive (2024)	11 / 11	3276	<ul> <li>Currently offline – Last data available on July 2024 (no prior issues). Suspected datalogger transmission issue.</li> </ul>	19,
SD-VTS-510-KT	5+10	Inactive (2024)	11 / 11	3260	<ul> <li>Offline for short periods in previous years (Appendix A)</li> <li>Currently offline – Last data available on July 2024. Suspected datalogger issue.</li> </ul>	19,
SD-HTS-510-US	5+10	Inactive (2024)	5/5	3274	<ul> <li>Damaged following construction (repaired)</li> <li>Offline for short periods in previous years (Appendix A)</li> <li>Currently offline – Last data available on July 2024. Suspected datalogger issue.</li> </ul>	19,
SD-HTS-B1-KT	NA	Inactive (2024)	20 / 20	3261	<ul> <li>Currently offline – Last data available on July 2024. Suspected datalogger issue.</li> </ul>	19,

Notes:

<sup>1</sup> The cables identified as Inactive (2024) have been reviewed and appear to not be recording the ground temperature. Through ongoing troubleshooting it is suspected that there is an issues with communications between the datalogger and GTCs and in some cases may be related to the discharging datalogger batteries.

The thermal design freezing point depression criteria requires a ground temperature of less than -2°C at the upstream base of the key trench (Figure 9). The ground temperatures meet the thermal design criteria with few exceptions, and the dam is performing as expected, as outlined in Table 4-8. Based on the operational GTCs, the thermal design criteria along the base of and in the foundation of the key trench is being met in all locations where data is available.

Thermal monitoring data for the GTCs are shown in Appendix A.

Zone	Horizontal GTC	Vertical GTC	Observation
Design Freezing Point Depression	−2°C	−2°C	The minimum criteria required to ensure Dam is performing in accordance with design specifications
Station 0+65	No GTC	Meets	Performing as expected with substantive safety buffer in the base of the key trench.
Station 1+55	Offline	Meets	Performing as expected with substantive safety buffer in the base of the key trench.
Station 2+40	Meets	Offline	Performing as expected with a small buffer on the horizontal for beads 1 and 2 and substantive safety buffer in the base of the key trench. No data collected after November 12, 2023 for the vertical cable at the base of a key trench.
Station 3+65	Meets	Offline	Performing as expected with small safety buffer on the horizontal key trench cable. SD-VTS-365-KT is irreparable.
Station 4+60	Offline	Offline	SD-HTS-460-KT and SD-VTS-460-KT offline as of July 19, 2024 (See Appendix A). Prior to the cables going offline, performance was as expected.
Station 5+10	No GTC	Offline	Performing as expected prior to cable SD-VTS-510-KT going offline July 19, 2024.
SD-HTS-B1-KT	Meets	N/A	Bead 2 (near station 2+40) exceed (are warmer than) the foundation freezing point depression seasonally, however no adverse performance is observed at Station 2+40 in the other GTCs

Table 4-8: Summary of K	ey Trench foundation	Ground Temperature	<b>Cable Observations</b>
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Each datalogger contains a photovoltaic cell which is intended to recharge the battery automatically however battery monitoring data (Appendix C) indicates that DL01A and DL03A show initial signs of discharging battery issues and is approaching 6V, which may result in dataloggers no longer recording ground temperatures or transmitting data.

#### **Recommendations:**

- New GTCs installed in November 2023 which are currently collected as spot readings, should be connected to dataloggers. Data collected/transmitted should be integrated into the overall monitoring system.
- Continue to investigate and troubleshoot the cables which stopped transmitting November 2023 and July 2024, to ensure that cables continue to function and data is collected. A minimum of monthly spot readings should be collected until the dataloggers are re-established. If connection with the dataloggers cannot be re-established consider replacing the dataloggers.
- Recharge, replace or repair the dataloggers or battery where the battery is draining. A drained battery may lead to stopped data transmission or datalogger malfunction.

- Protect any exposed cables or cables with limited gravel cover that may be prone to damage from snow clearing and other activities. Placement of boulders or other barricades as needed.
- Inspect the South Dam after spring melt, especially looking for any exposed or damaged ground temperature cables. This will allow for preventative maintenance and placement of protective material to be done if exposed cables are observed, which will help to limit the potential for damage from wildlife.

### 4.3.3 Survey Monitoring Points

Survey monitoring at the South Dam includes 12 crest survey monitoring points (SMPs), 3 deep settlement points (DSPs), and 19 surficial survey monitoring points (SSPs). For the 2024 monitoring period, four surveys were conducted for the surficial survey monitoring points in May, June, August, and September. Only one survey was conducted for the deep settlement points in June, and three surveys were conducted for the crest survey monitoring points in May, June, and August. Complete survey data is presented in Appendix E.

The overall vertical and horizontal displacement since August 2019 is limited in all survey locations. Measured displacements have substantial variability, for example in June 2023, however this is attributed primarily to survey error and inconsistent survey data collection. The magnitude of the overall displacement trends remains small and are not of concern.

For 2024, the following observations have been made:

- SSP: There is variability in all displacement measurements (survey variability), but no overall trends are observed. SD-SSP-08 and SD-SSP-06 are showing a trend of vertical displacement approaching -0.1 m, however limited readings were collected in 2024.
- DSP: There is limited variability in the displacement readings and no credible trend observed, particularly as only one survey of the DSP locations was collected.
- SMP: Only three surveys were collected and no elevation data was provided in August. For SD-SMP-09, horizontal displacement has exceeded 0.1 m in the latest data and will continue to be monitored, however no signs of displacement were observed near this point and the displacement is not corroborated by other nearby survey points.

A detailed aerial image and LiDAR survey was collected in September 2024 and will be reviewed in early 2025.

#### **Recommendation:**

- Survey frequencies, completeness and accuracy of surveys require improvement.
- Review and document existing tension crack length using recent aerial LiDAR and imagery, and GPS ground survey for future tracking of progression.

### 4.3.4 Visual Inspection

Visual inspections of the South Dam are required weekly when the TIA water level is below the full supply level. All weekly visual inspection reports, including photos, are maintained by AEM on an internal system and are not provided in the AGI. The visual inspection report and track changes to the dam surface, visible damage to instrumentation, signs of erosion or seepage, or any other surface anomalies.

### **Recommendation:**

No recommendations.

### 4.3.5 Monitoring of Water at the Toe of the South Dam

The South Dam seepage and ponded water monitoring program is described in the OMS (AEM, 2024). The program includes routine water quality sampling and flow measurements if flowing water is observed. Since dam construction in 2019, there has been no flowing water observed at the downstream toe of the South Dam. The purpose of the ponded water monitoring program is to establish a geochemical baseline and monitor for potential seepage or changes in thermal regime of the ice-rich tundra in the area. SRK's annual review of the 2024 geochemical monitoring data is ongoing and will be reported separately.

### **Recommendations:**

No recommendations.

## 4.4 Interim Dike & Spillway

The Interim Dike was constructed in 2023 as a replacement to the Aquadam, as described in Section 2.3.5. The Interim Dike was inspected during the AGI for the second time by SRK since construction and the primary observations are as follows:

- The maximum operating water level for the Saline Pond must account for the lower crest elevation of the Interim Dike.
- Aquadam trench has been re-sloped to mitigate immediate hazards (unstable ground). However consider filling the trench to limit potential thawing impacts.
- Tension cracks were observed on the upstream (south) crest of the Interim Dike in 2023. These cracks are expected as the 2H:1V rockfill dike slope is constructed on thawing, unconsolidated and ice-rich tailings. During the 2024 inspection the tension cracks appear similar to 2023.
- Based on the September 2024 LiDAR survey, the crest elevation appears lower than in 2023. The key elevations above the GCL crest should be checked using GPS RTK survey and the critical elevations of the structure updated in the OMS manual.

Monitoring of the Interim Dike is currently limited to visual inspections, opportunistic topographic surveys and GTC spot readings. It is important that a comprehensive and consistent monitoring

program be implemented and documented in the OMS manual. The monitoring program should including ground temperature monitoring, visual inspections, survey displacement monitoring, and water level monitoring in the Saline Pond, while considering the overall water management strategy.

Overall, the Interim Dike performance is satisfactory and in line with expectations. Diligent monitoring and maintenance will be important to maintain and extend the structure's lifespan.

The Interim Dike WECC was constructed in 2023 and was inspected during 2024 AGI walkover. The following observations were made:

- The WECC is currently blocked by a rock fill access road. This access road is intended to have culverts installed however this was not completed during construction of the road and therefore requires active management of the Saline Pond water levels by pumping and may require breaching of the road fill in order to avoid overtopping of the Interim Dike during a flood event.
- The WECC has been constructed with zones of rock armor which are thinner than designed, including areas where the non-woven geotextile is protruding along the WECC alignment.
- The WECC side slopes exhibit signs of hydraulic erosion and differential settlement likely linked to ice wedges and lateral water flow into the WECC.
- Construction overburden piles near the WECC inlet have been cleaned up and have reduced the ponding in this area.
- The saline water pond is being maintained at a low level (32.65 cm at the time of the inspection), and the spillway is inactive.
- Overburden piles have been regraded this year, and major ponding has been drained.

Photolog 7 and 9 provide a general overview of the Interim Dike, Spillway, and WECC conditions at the time of the AGI.

### **Recommendations:**

- A thorough inspection and detailed topographic survey of the Interim Dike should be carried out following freshet 2025.
- Implement the monitoring program for the Interim Dike (Table 4-3) including monitoring of displacement, foundation thermal conditions, water level in the Saline Pond (south side of the dike) and maintaining of the required beach at the South Dam.
  - The GTC data is currently collected as spot readings. Once dataloggers are in place, they should be downloaded monthly or transmitted automatically while the structure is operational, or until the thermal regime is well understood. Ideally, the dataloggers should be connected to the overall telemetry system and integrated into the monitoring platform.
  - An annual survey would ideally be captured as LiDAR or photogrammetry with orthomosaic imagery to provide a detailed and accurate topographic and visual record. Alternatively, a highdensity ground survey using RTK GPS could be collected.

- The operating water level of the Saline Pond should be adjusted to 34.3 masl, to reflect the invert of the WECC and settlement of the southern side of the dike. Consider the impacts of reduced Saline Pond capacity in the water balance.
- Following annual (minimum) topographic survey of the dike, the operating water level should be reviewed and adjusted if settlement is observed.
- The Interim Dike and WECC was constructed on frozen unconsolidated tailings and are sensitive to foundation thaw. In order to maximize the lifespan, the trench left by the thawed Aquadam bladder should be backfilled in 2025. This will thermally protect the north rock berm which supports the GCL containment layer.
- Settlement is expected if the foundation thaws. Due to the level of expected maintenance which may be required (typically following freshet), consider planning for these maintenance activities.
- Tension cracks observed should be visually monitored for indications of additional or progressive slumping and repaired if observed. Vehicle or equipment traffic should be directed to remain at least 3 meters back from the crest of the dike to avoid additional loading.
- If tailings are farmed from the tailings beach during the winter or spring, a grading or farming plan should be in place to avoid unintended impacts to the Interim Dike.

# 4.5 Tailings Deposit

The mine is currently in Care and Maintenance, as such no new tailings have been deposited within the TIA.

Tailings were borrowed from the tailings beach, to obtain the tailings required for the core of the Interim Dike. The borrowed tailings areas were at least 100 m from the toe of the South Dam. Maintaining a 100 m beach from the South Dam, such that the saline or reclaim pond is more than 100 m from the dam is an important operational consideration (AEM 2024).

Water quality monitoring at TL-13 (the Saline Water Storage sampling location) indicate a maximum chloride concentration of 12,300 mg/L CI and salinity of 20 psu in April 2024 (potentially impacted by cryoconcentration) and 5,520 mg/L CI and salinity of 9.3 psu in August 2024<sup>1</sup>. Following freshet, the minimum chloride concentration was 757 mg/L CI and salinity of 1.4 psu in May 2024. The elevated chloride concentrations are expected to have limited impact on the long-term tailings beach freezeback as the concentrations fluctuate annually and the ingress of saline water into the partially frozen tailings beach is expected to be limited. The Saline Water Storage is maintained at least 100 meters from the South Dam, which further mitigated the potential impact to the tailings beach. Impounded saline water at the Interim Dike may increase thaw settlement and performance over time.

<sup>&</sup>lt;sup>1</sup> For reference, during operations the threshold for tailings porewater of 4,500 mg/L CI equivalent to limit beach freezing point depression to 0.5°C.

### **Recommendations:**

No recommendations.

# 4.6 Emergency Dump Catch Basins (EDCB)

The Eastern Dump Catch Basin is in good condition as shown in Photolog 12 and 13. The Western Dump Catch Basin, however, has a wrinkled liner that does not appear to be adequately anchored, and therefore, may not perform as intended. Since the site is in Care and Maintenance this is not currently a concern. In general, East EDCB in good condition, only minor tension cracking noted on the crest of berm. West EDCB appears to be in similar condition as past years with settlement and tension cracking very visible along crest.

### **Recommendations:**

- No changes to the past recommendations.
  - The Western Emergency Dump Catch Basin still requires repairs. These repairs should be completed prior to restarting operations and tailings deposition. Additional liner slippage since 2020 was noted at the top of the liner crest. Further liner slippage may result in a reduction of the capacity of this emergency catch basin.
  - A ground survey of the EDCB (including the top elevations of the exposed liner) should be completed prior to resuming operations to verify LiDAR survey elevations and check of the available containment capacity of this catch basin.
  - Consider mechanical alternatives [to catch basins], such as pigging the line, to push tailings to the TIA in the event of a breakdown.

## 4.7 TIA Shoreline

Degradation of the natural ground has been observed below the high-water level, approximately 33 masl. This is mainly occurring on the sandy banks along the eastern edge of the reclaim pond and generally more pronounced on the northern aspects, influenced by the longer fetch distance along the pond (north-south). There are no indications of retrogressive thaw at this time; only erosion from wave action has been noted, primarily along sandy shoreline deposits. This erosion has revealed a potential sand source within the TIA, with a significant spatial extent. Photolog 10 and 11 present a general overview of the TIA Shoreline inspection.

### **Recommendations:**

 Visually inspect the shoreline from a helicopter and/or drone aerial photo to confirm no retrogressive thaw slumps have occurred.

# 4.8 Doris Creek Bridge

The Doris Creek Bridge provides the only access route to the TIA and is an important component of site infrastructure. Overall, no significant changes have been observed in the area. The bridge footings and abutments are in good condition and no signs of differential settlement or erosion are observed. However, the ground temperature cable connections are damaged and have not been read since November 2023. The cable connections must be repaired to maintain monitoring of the permafrost conditions underlying the bridge abutments. An overview of the Doris Bridge inspection can be found in Photolog 14 and 15.

### **Recommendations:**

 Repair or replace the ground temperature cable connections to ensure continuity of monitoring of the abutments, as required by the Water License.

# 4.9 Pipelines (Reclaim, Tailings Deposition and TIA Discharge)

Pipelines are placed directly on the ground, which could be either rockfill pads, road shoulders or directly on the tundra. There are signs of vegetation dieback because of pipelines placed directly on the tundra near the TIA. This is becoming a preferred flow path for surface runoff which could ultimately lead to surface erosion and subsequent thermal erosion of permafrost. At the time of inspection, no thermal or hydraulic erosion was observed.

### **Recommendations:**

- No changes to the past recommendations.
  - Agnico Eagle should carefully inspect all pipelines placed directly on the tundra for signs of vegetation dieback and associated flow path channeling. Where this is occurring, the pipeline must be relocated to follow existing all-weather road shoulders, and appropriate remediation needs to be put in place where damage has occurred.
  - The smaller diameter TIA pipelines going from the North Dam to Doris Creek, that were used during the care and maintenance period and before tailings were placed in the TIA around 2017, are no longer connected or functional. Agnico Eagle should consider removing these nonfunctional pipelines from the tundra.
  - Going forward, Agnico Eagle should consider abandoning the practice of placing pipelines directly onto the tundra. Additional pipelines (specifically any pipelines that are no longer in use) should be removed from the tundra where practical. Any pipeline removal should consider approaches to ensure that additional permafrost damage does not result from the removal activities.

## 4.10 TIA Reclaim System and Water Treatment Plant (710 Pumphouse)

There are no current geotechnical concerns with the new location of the reclaim pumphouse or the Water Treatment Plant pad (Figure 2).

In the reclaim jetty area, the pipelines are largely removed and most of the waste cleaned up. However, disturbances in the tundra, such as dozer tracks and overstripping below the Water Treatment Plant (WTP), pose a risk as they could become preferential flow paths or areas of ponding, potentially leading to further degradation.

To mitigate these issues, it is recommended to backfill the overstripped toe below the WTP slope with Run-of-Quarry (ROQ) material. Additionally, monitoring the dozer tracks for signs of increased thermal erosion should be completed, and ideally rock fill should be placed within the track marks to limit ponding.

### **Recommendations:**

- Backfill the overstripped toe below the WTP slope with Run-of-Quarry (ROQ) material.
- Monitor the dozer tracks for signs of increased thermal erosion, and rock fill should be placed within the track marks to limit ponding.

# 4.11 TIA Operational Water Balance and Level Targets

The TIA operational water and load balance tool is used to predict water levels in the TIA and communicate water balance updates and projections monthly. The normal operation water level target for 2024 was less than 34.0 masl, however the maximum water level in 2024 was 32.12 masl in January, decreasing to 30.70 by the end of 2024.

The strong focus by AEM on water management in 2024 is acknowledged, it will be important to integrate the current water management strategy with the findings from the ongoing review of the North Dam thermal performance and any additional modelling which may inform changes to the water level TARPs or OMS.

### **Recommendations:**

- No changes to past recommendations:
  - Review the TIA operating water levels and the associated water level TARPS annually, in conjunction with the result of the ongoing North Dam thermal performance monitoring and analysis.

## 4.12 Climate Data

For reference, the updated climate data received from the Doris meteorological station is provided in Appendix G. The data presented summarizes the historical climate record and the 2024 climate record. The climate data is reviewed by Stantec and then distributed to Agnico, and SRK. SRK maintains a climate record in the Environmental Data Management System database.

# **5** Recommendations and Conclusions

Based on the results of the 2024 AGI, the Doris TIA and associated structures (primarily the North Dam and South Dam) are functioning as designed. The Interim Dike is performing well; however some additional maintenance monitoring is recommended. Table 5-1 presents a summary of the recommendations listed throughout this report.

Area	Inspection Item	Observation	Recommendation	Recommendation ID
General TIA	Tailings Operating, Maintenance and Surveillance (OMS) Manual and Emergency Response Plan (ERP)	<ul> <li>Interim Dike and South Dam toe Berm constructed in 2023 and new instrumentation was installed.</li> <li>Modifications to the monitoring systems are not fully captured with</li> </ul>	• <b>COMPLETED:</b> Update the OMS manual to include the Interim Dike as-built details and Interim Dike monitoring SOP, Saline Pond management and any changes to the water management strategy or operating criteria related to the Interim Dike.	2023-AGI-01
			<ul> <li>Update the monitoring SOPs for the North and South Dam to reflect all current monitoring instrumentation and procedures.</li> </ul>	
			Update the OMS manual to include any of the changes/revisions not captured in the current version of the OMS, including the South Dam toe berm, Emergency Overflow Channel implementation timing and any changes because of the dam hazard classification review.	
			<ul> <li>OMS Manual, TARPs and Emergency Response Plan should be reviewed with the Agnico Eagle site staff annually, or after revisions; to ensure staff are appropriately informed and trained on the contents of these documents.</li> </ul>	
	Independent Dam Safety Review and Risk Assessment	<ul> <li>DSR recommendations are being addressed where appropriate.</li> </ul>	<ul> <li>Continue to address recommendations from the DSR, where appropriate.</li> </ul>	2023-AGI-02
		<ul> <li>Independent review board meetings were held in July 2024.</li> </ul>	<ul> <li>In line with recommendations from the DSR, the dam hazard classification should be reviewed and updated prior to resuming operations, and the review should consider the 2023 CDA</li> </ul>	

### Table 5-1: Table of Recommendations

Area	Inspection Item	Observation	Recommendation	Recommendation ID
			Technical Bulletin on Environmental Consequence Classification.	
	Compliance with Monitoring Frequency Requirements	<ul> <li>Some visual inspection, survey monitoring missed, however overall compliance is acceptable.</li> </ul>	<ul> <li>Recommended monitoring frequencies have been met in most categories, however:         <ul> <li>Three survey monitoring events we missed due to issues with the survey equipment (these have been addressed for 2025).</li> <li>Some of the newly installed ground temperature cables on the North and South Dam are read infrequently and existing dataloggers have stopped transmitting. AEM have attempted repair and replacement. Some transmission issues remain.</li> <li>AEM should aim to improve the frequency of monitoring in 2025.</li> </ul> </li> <li>Formalize and implement the monitoring program for the Interim Dike.</li> <li>Update the OMS manual and monitoring SOPs to include any new or updated instrumentation</li> </ul>	2023-AGI-03 (updated)
North Dam	Overall (Visual) Inspection of the North Dam during AGI	<ul> <li>Disturbance above the west abutment toward the Emergency Overflow Channel (EOC) alignment due to drill tracks was observed in 2022 (Drilling for EOC).</li> <li>Tundra die-back was observed along the eastern upstream toe of the dam, below the high-water mark. This area should be monitored closely over the next year for signs of thermal erosion and increased thaw settlement.</li> </ul>	<ul> <li>Previous recommendations unchanged.</li> <li>Additional recommendations include:</li> <li>Disturbance (track marking) on the tundra above the west abutment, due to drilling access during the EOC drilling investigation was previously noted (SRK, 2023b). This area was inspected and no signs of erosion or permafrost degradation were observed in 2024, however the areas should continue to be monitored periodically and mitigation measures implemented if changes are observed.</li> <li>Tundra dieback observed along the upstream toe (below 33.05 masl, the maximum water Reclaim Pond level) should include monitoring</li> </ul>	2022-AGI-08

Area	Inspection Item	Observation	Recommendation	Recommendation ID
			for erosion or increased permafrost thaw settlement in the future.	
	Ground Temperature Cables (GTCs)	<ul> <li>An accelerated and credible warming trend in GTC beads on the upstream side of the core was observed in late 2023. This trend is Expected to be related to historically high-water levels.</li> </ul>	<ul> <li>Continue to closely monitor warming conditions along upstream side of the North Dam and continue to monitor the results, adhere to the TARPs, plan/implement additional review meetings, analysis and implement responses/mitigations accordingly.</li> <li>Continue downloading data every two weeks until observed warming conditions subside.</li> </ul>	2023-AGI-04
		<ul> <li>New GTCs installed on the upstream face which are nor connected to dataloggers should be monitored regularly (minimum of monthly)</li> <li>Thermal readings from a ground temperature cable within an uncovered PVC pipe will not be representative of the boundary condition of the upstream dam face, above the water level.</li> </ul>	<ul> <li>Consider implementing dataloggers for all new GTCs, and continue manual spot readings until dataloggers are installed.</li> <li>Cover the dam face GTCs with non-woven geotextile and a thin layer of rock for protection and to improve the quality of the temperature readings.</li> </ul>	2024-AGI-23
	GTC Datalogger Battery	<ul> <li>GTC datalogger batteries have not been charged since 2022, and CR-1000#2 is below the recommended voltage of 12.0V</li> </ul>	<ul> <li>Recharge the CR-1000 Batteries as the voltage of CR-1000#2 Battery is below 12.0V</li> </ul>	2024-AGI-24
	Thermosyphons	<ul> <li>The passive thermosyphon system was converted to a hybrid thermosyphon system in 2024</li> <li>The active cooling unit on the south thermosyphons was not operational in the fall of 2024 and should be repaired prior to spring 2025. AEM is planning to have AFC come to site to troubleshoot.</li> </ul>	<ul> <li>Troubleshoot and repair the active refrigeration system prior to the end of the passive thermosyphon cooling period (Typically ending in April)</li> <li>Update the OMS to include considerations for the operations, maintenance and monitoring of the hybrid thermosyphon cooling system.</li> <li>After at least one full season of operation, review the performance of the active cooling</li> </ul>	2024-AGI-25

Area	Inspection Item	Observation	Recommendation	Recommendation ID
			system and assess the effectiveness of the system.	
	Inclinometers	<ul> <li>Inclinometer grooves appear to be rotated slightly from the expected position of parallel and perpendicular to the crest.</li> <li>Baseline orientation measurements were collected during the 2024 AGI.</li> </ul>	<ul> <li>Updated recommendation: Record the inclinometer casing groove directions annually for at least three years to verify if there is any ongoing rotation. Take groove direction readings relative to the line of inclinometer casings (perpendicular to crest).</li> </ul>	2023-AGI-05
		<ul> <li>Inclinometer probe yielding erroneous results and requiring lengthy repair/calibration period.</li> </ul>	<ul> <li>Consider installation of automated inclinometer readings, via in place inclinometer (IPI) or shape accel array (SAA) to improve precision, continuity and reduce gaps associated with long inclinometer probe repair periods.</li> </ul>	Comment
	Survey Monitoring Points	<ul> <li>New upstream monitoring points were installed in 2023 and are being monitored</li> </ul>	<ul> <li>Integrate new upstream surficial survey points into the North Dam monitoring SOP and OMS.</li> </ul>	2023-AGI-06
		<ul> <li>Some survey points were damaged during snow clearing</li> </ul>	<ul> <li>Re-establish the surficial survey points that were damaged due to snow removal and install flags to prevent future damage when heavy equipment is working nearby.</li> </ul>	2024-AGI-26
	Monitoring of Water at the Toe of the North Dam	<ul> <li>V-notch weir remains in place but does not provide an accurate measurements due to flow depth and bypassing flow.</li> </ul>	The v-notch weir at the toe of the dam does not provide accurate flow measurements. Consider decommissioning if disturbance to the toe of the dam can be minimized, or it may be left in place provided no signs of thermal degradation at the toe are observed.	2023-AGI-07
			<ul> <li>If a change in typical water flow rates is observed (subjective) this should be noted on the visual inspection form.</li> </ul>	
South Dam	Annual (Visual) Inspection of the South Dam during AGI	<ul> <li>The South Dam toe berm was constructed in May 2023. It covered the extents of the</li> </ul>	<ul> <li>The Phase 2 abutment tension cracks (outside of the lateral Phase 1 tailings extent) should continue to be monitored and plans to mitigate</li> </ul>	2023-AGI-08

Area	Inspection Item	Observation	Recommendation	Recommendation ID
		relaxation and tension cracks along the South Dam, across the Phase 1 tailings extent. Tension cracking on the downstream face of the Phase 2 abutments remain.	this if the cracking progresses to the point where progressive thaw slumps could be expected.	
		<ul> <li>Past tailings borrow source for Interim Dike has lead to ponding on beach closer than previously observed, it is currently more than 100 m from the dam.</li> </ul>	<ul> <li>Avoid tailings excavation or farming within 100 m of South Dam to maintain beach lengths</li> </ul>	2023-AGI-09
		<ul> <li>Tailings dust has been observed downstream of the tailings dam, outside of the South Dam catchment.</li> </ul>	<ul> <li>Continue the tailing dust related monitoring program and consider adding dust fall monitoring as appropriate.</li> </ul>	2024-AGI-##
			<ul> <li>Dust mitigation on the southern extents of the beach should be considered until deposition is planned to be resumed.</li> </ul>	
	Ground Temperature Cables (GTCs) and Dataloggers	<ul> <li>Replacement of damaged vertical GTCs occurred in November 2023. Additionally, a GTC was installed upstream of the dam, in</li> </ul>	<ul> <li>New GTCs installed in November 2023 should be protected and connected to dataloggers. Data collected/transmitted should be integrated into the overall monitoring system.</li> </ul>	2023-AGI-10
		the tailings beach.	<ul> <li>Ensure the new and existing datalogger transmission subscriptions are maintained.</li> </ul>	
		<ul> <li>A number of cables stopped transmitting simultaneously on July 19, 2024. No obvious signs of damage were observed during the inspection and the problem is expected to be on the datalogger transmission side. AEM and Beadedstream should continue to troubleshoot the issue.</li> </ul>	Continue to investigate and troubleshoot the cables which stopped transmitting during since November 2023 and July 2024 to ensure that cables are maintained, and data is collected. A minimum of monthly spot readings should be collected if the dataloggers are not re- established.	2024-AGI-27
		<ul> <li>Battery monitoring data (Appendix C) indicates that DL01A and DL03A show initial signs of</li> </ul>	<ul> <li>Recharge, replace or repair the dataloggers or battery where the battery voltage is draining. A drained battery may lead to stopped data transmission or datalogger malfunction.</li> </ul>	2023-AGI-11 (updated)

Area	Inspection Item	Observation	Recommendation	Recommendation ID
		discharging battery issues and is approaching 6V.		
		<ul> <li>GTC cable alignments currently protected by thin layer of crushed rock with limited protection from snow clearing equipment.</li> </ul>	<ul> <li>Protect any exposed cables or cables with limited gravel cover that may be prone to damage from snow clearing and other activities, by placement of boulders or other barricade.</li> </ul>	2023-AGI-12
			<ul> <li>Inspect the South Dam after spring melt, especially looking for any exposed or damaged ground temperature cables. This will allow for preventative maintenance and placement of protective material to be done if exposed cables are observed, which will help to limit the potential for damage from wildlife.</li> </ul>	
	Survey Monitoring	<ul> <li>LiDAR and aerial imagery were collected in September 2024 which provide adequate documentation of the existing tension cracks.</li> </ul>	<ul> <li>Review and document existing tension crack lengths using recent aerial LiDAR and imagery, and GPS ground survey for future tracking of progression.</li> </ul>	2023-AGI-13 (updated)
		<ul> <li>Some monthly surveys were not completed and there were some data quality issues in the provided survey data.</li> </ul>	<ul> <li>Survey frequencies and completeness and quality of surveys require improvement.</li> </ul>	2024-AGI-28
Interim Dike	Interim Dike	<ul> <li>Tension cracks and slumping has been repaired along the Aquadam trench, however the trench has not been backfilled.</li> <li>Tension cracks were observed along the south crest of the Interim</li> </ul>	<ul> <li>The Interim Dike and WECC was constructed on frozen unconsolidated tailings and are sensitive to foundation thaw. In order to maximize the lifespan, the trench left by the thawed Aquadam bladder should be backfilled. This will thermally protect the north rock berm</li> </ul>	2023-AGI-15 (updated)
		Dike.	<ul> <li>which supports the GCL containment layer.</li> <li>Settlement is expected if the foundation thaws. Due to the level of expected maintenance which may be required (typically following freshet), consider planning for these maintenance activities.</li> </ul>	
			<ul> <li>Tension cracks observed should be visually monitored for indications of additional or</li> </ul>	

Area	Inspection Item	Observation	Observation Recommendation	
			progressive slumping and repaired if observed. Vehicle or equipment traffic should be directed to remain at least 3 meters back from the crest of the dike to avoid additional loading.	
		<ul> <li>The Interim Dike construction was completed in 2023.</li> <li>Additional GTC monitoring instrumentation was installed in November 2023.</li> <li>A monitoring program has been established in the OMS manual (AEM 2024)</li> </ul>	<ul> <li>A thorough inspection and detailed topographic survey of the Interim Dike should be carried out following freshet to observe how the structure performed, following a full year of operations.</li> <li>Implement the monitoring program for the Interim Dike (Table 4 3) including monitoring of displacement, foundation thermal conditions, water level in the Saline Pond (south side of the dike) and maintaining of the required beach at the South Dam.</li> <li>The GTC data is currently collected as spot readings. Once dataloggers are in place, they should be downloaded monthly or transmitted automatically while the structure is operational, or until the thermal regime is well understood. Ideally, the dataloggers should be connected to the overall telemetry system and integrated into the monitoring platform.</li> <li>An annual survey would ideally be captured as LiDAR or photogrammetry with orthomosaic imagery to provide a detailed and accurate topographic and visual record. Alternatively, a high-density ground survey using RTK GPS could be collected.</li> <li>The operating water level of the Saline Pond should be adjusted to 34.3 masl, to reflect the invert of the WECC and settlement of the southern side of the dike. Consider the impacts of reduced Saline Pond capacity in the water balance.</li> <li>Following annual (minimum) topographic survey of the dike, the operating water level</li> </ul>	2023-AGI-16 (updated)

Area	Inspection Item	Observation	Recommendation	Recommendation ID
			should be reviewed and adjusted if settlement is observed.	
	Interim Dike Water Elevation Control Channel (WECC)	<ul> <li>Previous excavated material piles have been regraded.</li> <li>The Interim Dike crest height varies and is below the original design elevation.</li> <li>The WECC is blocked by a newly installed access road. Culverts were designed but not installed.</li> </ul>	<ul> <li>The Interim Dike and WECC was constructed on frozen unconsolidated tailings and are sensitive to foundation thaw. In order to maximize the lifespan, the trench left by the thawed Aquadam bladder should be backfilled in 2025. This will thermally protect the north rock berm which supports the GCL containment layer.</li> <li>Settlement is expected if the foundation thaws. Due to the level of expected maintenance which may be required (typically following freshet), consider planning for these maintenance activities.</li> <li>Tension cracks observed should be visually monitored for indications of additional or progressive slumping and repaired if observed. Vehicle or equipment traffic should be directed to remain at least 3 meters back from the crest of the dike to avoid additional loading.</li> <li>The spillway is obstructed by a road without culverts, necessitating the pond to be kept low enough to accommodate the freshet. It's important to check the elevation of the dike and assess storage capacity.</li> <li>If tailings are farmed from the tailings areabeach of overburden piles during the winter or spring, a grading or farming plan should be in place to avoid unintended impacts to the Interim Dike.</li> </ul>	2023-AGI-17 (updated)
Other TIA Areas	Emergency Dump Catch Basins	<ul> <li>No modifications to the EDCB have been made.</li> </ul>	<ul> <li>No changes to the past recommendations.</li> </ul>	2022-AGI-13
	TIA Shoreline	<ul> <li>Degradation of the natural ground has been observed below the</li> </ul>	<ul> <li>Visually inspect the shoreline from a helicopter and/or drone aerial photo to confirm no retrogressive thaw slumps have occurred.</li> </ul>	2024-AGI-29

Area	Inspection Item	Observation	Recommendation	Recommendation ID
		high-water level, approximately 33 meters above sea level (masl).		
	Doris Creek Bridge	<ul> <li>The bridge abutment condition appears unchanged.</li> <li>GTC SRK10-DCB1 and SRK 10-DCB2 read out connections were damaged after the November 2023 and July 2023 readings, respectively.</li> <li>The gabion baskets which form part of the bridge abutment structure are deformed (and have been since construction), and therefore it is not possible to tell if additional deformations of the gabion wall have occurred. However this gabion wall only retains road fill.</li> <li>Some tension cracks were noted along the edge of the turnout near the bridge.</li> <li>No signs of deformation or settlement below the abutment are observed.</li> <li>Ground temperature cable connections are still damaged.</li> </ul>	<ul> <li>Repair or replace the ground temperature cable connections, or check the cable and connect it to a datalogger to ensure continuity of monitoring of the abutments, as required by the Water License</li> </ul>	2024-AGI-30
	Pipelines (Reclaim, Tailings Deposition and TIA Discharge)	<ul> <li>Unused pipelines on tundra</li> <li>Vegetation dieback under pipelines</li> </ul>	<ul> <li>No changes to the past recommendations.</li> </ul>	2023-AGI-19
	TIA Reclaim System and WTP (710 Pumphouse)	<ul> <li>The water treatment plant (WTP) has been constructed and commissioned and the 710 Pumphouse has been relocated to the new Reclaim Pond pumping location near the WTP.</li> </ul>	<ul> <li>Backfill the over stripped toe below the WTP slope with Run-of-Quarry (ROQ) material.</li> </ul>	2023-AGI-20 (updated)

Area	Inspection Item	Observation	Recommendation	Recommendation ID
		<ul> <li>Substantial ruts in tundra (heavy equipment tracks) and areas of over-stripping with ponded and slowly flowing water was observed near the new WTP.</li> </ul>	<ul> <li>Monitor the dozer tracks for signs of increased thermal erosion, and rock fill should be placed within the track marks to limit ponding.</li> </ul>	
	TIA Operational Water Balance and Level Targets	<ul> <li>The TIA operational water levels and TARPs have been revised.</li> <li>Operation of the Water Treatment Plant was able to lower the water level to 30.7 by the end of 2024</li> <li>High water levels are thought to be a cause of the upstream core warming at the North Dam.</li> </ul>	<ul> <li>No changes to the past recommendations</li> </ul>	2023-AGI-21

2024 Annual Geotechnical Inspection – Doris Tailings Impoundment Area Closure

# Closure

This report, 2024 Annual Geotechnical Inspection - Doris Tailings Impoundment Area, was prepared by

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ter ter film film filme ter ter a

Anton Novikov, EIT Staff Consultant

and



Peter Luedke, PEng Senior Consultant

and reviewed by

This signatury Splin exclusive u authorized.

Megan Miller MEng, PEng Principal Consultant

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Date _	2025	1-3/2	4
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N I	Engineers and	d Geoscie	essional ntists

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All data used as source material plus the text, tables, figures, and attachments of this document have been reviewed and prepared in accordance with generally accepted professional engineering and environmental practices.

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Figures



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#### LEGEND

- As-Constructed Infrastructure
- Proposed Infrastructure
- Quarries
- Reclaim Pond Extent
- Saline Pond
- Subaerial Tailings Beach (2021)
- Ultimate Reclaim Pond Extent
- Ultimate Tailings Extent

#### NOTES

1. All units are in meters unless otherwise specified.

#### REFERENCES

NAD83 CSRS UTM Zone 13.

ESRI World Imagery, retrieved December 20, 2024.

Hope Bay 2024 Mosiac, provided by client.

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### Doris General Arrangement

Hope Bay

DATE:	
February 2025	

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SRK JOB NO.:	CAPR003066	Hope Bay
ILE NAME:	CAPR003066 - Doris TIA.dwg	поре вау

### LEGEND

	Existing Infrastructure Permitted Infrastructure (Not Constructed)
	Quarry
[_]	Ultimate Reclaim Pond Extent
	Ultimate Tailings Extent
	Watershed Boundary

#### NOTES

1. All units are in meters unless otherwise specified.

#### REFERENCES

NAD83 UTM Zone 13. NAD83 CSRS UTM Zone 13. Hope Bay 2024 Mosiac, provided by client. Tailings Beach survey collected by drone LiDAR in August 2021, data provided by client.

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	2024 Annual	Geotech	nical Insp	ection
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		)		
	o	Thermosyphon Evaporator Pipe		
		(NTS) - Natural Ground		
		Stratigraphic Boundary		
		Geosynthetic Clay Liner (GCL)		
		Core Material		
		Kev Trench		
		GCL Cover Material		
		Transition Material		
		ROO Material		
		Thermosyphon Evaporator Pipes		
		Thermosyphon Evaporator Pipes		
		Core Material		
		Transition Matorial		
		Pup of Ouerry (POO)		
		Rull of Quality (ROQ)		
		Веагоск		
		Peat		
	NOTES			
	r. me extr	apolated from a series of geotechnical		
	aug	er holes and shallow test pits. Bedrock		
	cont	tact and geological unit contacts are		
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	Upstream			
ESI EL 22.5m				
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	North D	am Foundation Conditions and		
	Typical As-Constructed Section			

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# LEGEND

8	Thermistor Bead Location
	Lower GCL Liner
	Upper GCL Liner
	Bedding Material
	Transition Material
	Run of Quarry Backfill

# NOTES

- 1. Topographic and as-constructed contour data from the terrain model was provided by the Client.
- 2. All units shown are in meters unless otherwise stated.

# REFERENCES

NAD83 UTM Zone 13.

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	South Dam Fo Typical As-	undatior Constru	Conditions	and
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# LEGEND

Ground Temperature Cable
Lower GCL Liner
Upper GCL Liner
Bedding Material
Transition Material
Run of Quarry Backfill

### NOTES

- 1. Topographic and as-constructed contour data from the terrain model was provided by the Client.
- 2. All units shown are in meters unless otherwise stated.

### REFERENCES

NAD83 UTM Zone 13.

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February 2025 PDL TO	February 2025	PDL		10



# LEGEND

	GCL Liner
	ROQ Material
$\square$	Filter / Bedding Material
	Key Trench Excavation
<i>77</i>	Compacted Tailings
	Abutment Cover

### NOTES

- 1. Topographic and as-constructed contour data from the terrain model was provided by the Client.
- 2. All units shown are in meters unless otherwise stated.

# REFERENCES

NAD83 UTM Zone 13.

	2024 Annual Geotechnical Inspection			
	Interim Dike Foundation Conditions and Typical Sections			
Норе Вау	DATE: February 2025	APPROVED: PDL	FIGURE:	11



Photo Logs





Photo 1: North Dam Overview from the Helicopter (Looking Southeast).





Photo 3: North Dam Downstream Face (Looking Southwest).



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Photo 5: North Dam Northeastern Thermosyphon (Looking Northwest).





Photo 7: North Dam Instrumentation Inspection (Looking Northwest).



Photo 8: North Dam Instrumentation Inspection (Looking Northwest).

		2024 TIA AGI		
<b>Srk</b> consulting		North Dam Inspection		
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Photo 9: South Dam Overview from the helicopter (Looking Northwest).





Photo 11: North Dam Downstream Face (Looking Northwest).



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		AGNICO EAGLE	South Dam Inspection		
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Photo 13: South Dam Cracking Downstream Face (Looking Southeast).





Photo 15: South Dam Upstream Face (Looking Southwest).



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Photo 17: Interim Dike Overview from the helicopter (Looking Southeast).



Photo 19: Interim Dike Crest (Cracking) (Looking West).



Photo 18: Interim Dike Overview and Former Aquadam Location (Looking West).



Photo 20: Interim Dike Upstream Face (Cracking) (Looking West).

		2024 TIA AGI		
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Photo 21: Interim Dike Spillway (Looking South).



Photo 23: Interim Dike Spillway (Looking Southeast).





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Photo 25: TIA Shoreline Overview (Looking South).



Photo 27: TIA Shoreline Overview (Looking Northeast).





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SRK JOB NO: CAPR003066	
LAYOUT: CAPR003066_HB_2024_TIAAGI	



Photo 29: Eastern Emergency Dump Catch Basin (Looking Southeast).





Photo 31: Western Emergency Dump Catch Basin (Looking Northwest).



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Photo 33: Eastern Side of Doris Bridge, Northern Gabion (Looking South).





Photo 35: Eastern Side of Doris Bridge, Southern Gabion (Looking East).



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Photo 37: ROQ below the WTP slope (Looking Southeast).





Photo 39: Disturbance in Tundra (Dozer Tracks) (Looking Northwest).



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Appendix A Ground Temperature Cables



Bead 8

Bead 9 Bead 10

-30





	2024 TIA AGI		
	Station 0+40		
IICO EAGLE	Ground Temperature Cable		Cable
	<ul> <li>Temperature Vs. Time</li> </ul>		
Норе Вау	Date: Approved: Figure: A.1		



CAPR003066

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Job No:

Bead numbers increase from downstream to upstream (horizontal) and top to bottom (vertical).



GTC Status: Bead damaged or data missing

		2024 TIA AGI	
	Station 0+40		Cable
IICO EAGLE	Ground Temperature Cable     Readings by Location		tion
Hope Bay	Date: Oct. 2024 Approved: PDL Figure: A.2		





		2024 TIA AGI	
	Station 0+60 Horizontal Ground Temperature Cable		rature Cable
	nea nea	uniys by Loca	
Норе Вау	Date: Approved: Figure: A.4		Figure: A.4



- GTC Status: Bead damaged or data missing

	2024 TIA AGI		
	Station 0+60		
IICO EAGLE	Vertical Temp	erature Cable	Temperature
	Vs. Time		
Норе Вау	Date: Oct. 2024	Approved: PDL	Figure: A.5





ND-HTS-085-US Bead 1 40 Bead 2 Bead 3 35 Bead 4 30 Temperature (°C) Bead 5 25 Bead 6 20 Bead 7 15 Bead 8 Bead 9 10 Bead 10 5 Bead 11 0 Bead 12 -5 Bead 13 20-141-24 8.0Ct.7A Bead 14 18-0Ctr – Bead 15 ND-HTS-085-29.4





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# interval datasets from this reporting period.

- Previous Data were recorded between August 2012 and September 2023.
- · Bead numbers increase from downstream to upstream (horizontal) and top to bottom (vertical).
- Erroneous data attributed to instrumentation error have been omitted.
- Notable temperature increase observed in the upstream cables. This is expected to be related to historically high reclaim pond water levels in 2023-2024.

			2024 TIA AGI		
			Station 0+85		
		AGNICO EAGLE	Horizontal Ground Temperature Cable		
	CARRONNOC		iveaulings by Location		
JOD NO:	CAPR003066	Hone Bay	Date:	Approved:	Figure:
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Erroneous data attributed to instrumentation error have been omitted.



Date: Oct. 2024

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	2024 TIA AGI		
	Station 0+130 Horizontal Temperature Cable		re Cable
	l ieu	iperature vs. i	IIIIe
Норе Вау	Date: Oct. 2024	Approved: PDL	Figure: A.13



	Readings by Location		
lope Bay	Date:	Approved:	Figure:
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Erroneous data attributed to instrumentation error has been omitted.





	2024 TIA AGI		
	Station 0+175 Ground Temperature Cable Temperatu		Temperature
		vs. mile	
Норе Вау	Date: Oct. 2024	Approved: PDL	Figure: A.19



Date: Oct. 2024 pproved Hope Bay A.20 PDL









- Bead numbers increase from upstream to downstream (horizontal) and top to bottom (vertical).
- Measurements during construction were collected between April and July 2018, only data following final instrumentation commissioning (January 27, 2019) is shown.
- (A) No data collected between June 11, 2022 and August 15, 2022 for SD-HTS-065-US .
- (B) No data collected between June 11, 2022 and August 15, 2022 and between September 2, 2022 and October 16, 2022 for SD-VTS-065-KT.
- (C) No data collected after July 19, 2024 for SD-HTS-065-US.

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	0	AGN
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## Legend:

- GTC Status: Cable irreparably damaged
- GTC Status: Bead damaged or data missing

# SD-VTS-065-KT

		2024 TIA AGI	
	Station 0+65		
IICO EAGLE	Ground Temperature Cable		e Cable
	Temperature Vs. Time		
Норе Вау	Date: Jan 2025	Approved: PDL	Figure: A.21







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Date: Jan 2025

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GTC Status: Bead damaged or data missing



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**Irreparably Damaged** 2024 TIA AGI Station 1+55

ICO EAGLE	Horizontal Temperature Cable		
	Temperature Vs. Time		
Hope Bay	Date: Jan 2025	Approved: PDL	Figure: A.23



	2024 TIA AGI		
	Station 1+55		
IICO EAGLE	Ground Temperature Cable		
	Readings by Location		
Норе Вау	Date: Jan 2025	Approved: PDL	Figure: A.24



		2024 TIA AGI	
	Station 1+55		
IICO EAGLE	Vertical Temperature Cable		e Cable
	Temperature Vs. Time		
Норе Вау	Date: Jan 2025	Approved: PDL	Figure: A.25



	2024 TIA AGI			
	Station 1+55 Ground Temperature Cable		e Cable	
	Readings by Location			
Норе Вау	Date: Approved: Figure: Approved: Approve: Approved: Approved: Approved: Approved: Approved: App			



## Legend:

- GTC Status: Cable irreparably damaged
- GTC Status: Bead damaged or data missing





	2024 TIA AGI		
	Station 2+40		
IICO EAGLE	Ground Temperature Cable		
	Readings by Location		
Норе Вау	Date: Jan 2025	Approved: PDL	Figure: A.28



	2024 TIA AGI		
	Station 2+40		
IICO EAGLE	Vertical Temperature Cable		e Cable
	Temperature Vs. Time		Time
Норе Вау	Date: Jan 2025	Approved: PDL	Figure: A.29





		2024 TIA AGI	
	Station 3+65		
IICO EAGLE	Horizontal Temperature Cable		ire Cable
	Temperature Vs. Time		
Норе Вау	Date: Jan 2025	Approved: PDL	Figure: A.31





# GTC Status: Bead damaged or data missing

	2024 TIA AGI		
	Station 3+65		
IICO EAGLE	Vertical Temperature Cable		
	Temperature Vs. Time		
Норе Вау	Date: Jan 2025	Approved: PDL	Figure: A.33



- No data collected between January 20, 2023 and March 11, 2023 for SD-VTS-365-US.
- No data collected after August 3, 2020 SD-VTS-365-DS. GTC assumed to be irreparably damaged.

Hope Bay

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Temperature Vs. Time

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Date: Jan 2025



	2024 TIA AGI		
	Station 4+60 Vertical Temperature Cable		e Cable
	Temperature Vs. Time		
Норе Вау	Date: Jan 2025	Approved: PDL	Figure: A.37





## Notes:

- Vertical and horizontal offset graphs display data in two-week intervals.
- Previous data were recorded between November 2018 and September 2023.
- Bead offset from centerline for SD-HTS-460-US is approximate.
- No data collected after July 19, 2024 for SD-HTS-460-KT and SD-VTS-460-DS.

		2024 TIA AGI		
-V-SFK consuling	AGNICO EAGLE	Station 4+60 Ground Temperature Cable		e Cable
		Readings by Location		ation
Job No: CAPR003066	Hone Pov	Date:	Approved:	Figure:
Filename: App_A_SD_GTC.pptx	норе Вау	Jan 2025	PDL	° A.38





GTC Status: Bead damaged or data missing



• Previous data were recorded between November 2018 and September 2023.

• No data collected after July 19, 2024 for SD-VTS-460-KT and SD-VTS-460-US.

Job No:

CAPR003066 Filename: App\_A\_SD\_GTC.pptx







# <del>──</del>2023-11-10 **—**2024-02-02 **→**2024-03-15 <del>~~</del>2024-03-29 <del>~~</del>2024-07-05 Max Previous Data ----Min Previous Data 2024 TIA AGI Station 4+60

IICO EAGLE	Ground Temperature Cable		
	1 Readings by Location		
Норе Вау	Date: Jan 2025	Approved: PDL	Figure: A.39





## Notes:

-15

-20

-25

-30

See note (A)

Bead numbers increase from downstream to upstream (horizontal) and top to bottom (vertical). •

See note (B

- Measurements during construction were collected between April and July 2018, only data following final instrumentation commissioning (November 6, 2018) is shown.
- (B) Data collection gaps between August 7, 2020 and September 11, 2020. •
- •
- (D) No data collected after July 19, 2024 for SD-VTS-510-KT and SD-HTS-510-US. •

	<b>srk</b> consulting	AGNICO EA
Job No: Filename:	CAPR003066 App_A_SD_GTC.pptx	Hope Bay

## Legend:

- GTC Status: Cable irreparably damaged
- GTC Status: Bead damaged or data missing

# SD-HTS-510-US



Date: Jan 2025

Temperature Vs. Time

ed: PDL

Ä.40



	Station 5+10		
NICO EAGLE	Ground Temperature Cable		e Cable
	Readings by Location		
Норе Вау	Date: Jan 2025	Approved: PDL	Figure: A.41



Job No:	CAPR003066	
Filename:	App A SD GTC.pptx	

		2024 TIA AGI	
	Key Trench		
NICO EAGLE	Horizontal Temperature Cable		
	Temperature Vs. Time		
Норе Вау	Date: Jan 2025	Approved: PDL	Figure: A.42





	2024 TIA AGI				
	Station 0+40				
IICO EAGLE	Ground Temperature Cable				
	Readings by Location				
Норе Вау	Date: Jan 2025	Approved: PDL	Figure: <b>A.44</b>		





ID-GTC-2





### Notes:

- Bead numbers increase from downstream to upstream (horizontal) and top to bottom (vertical).
- collection methods. Data gaps that fall within this reporting period can be attributed to infrequent manual collection of data.

		2024 TIA AGI		
		Station 1+10		
	AGNICO EAGLE	Vertical Temperature Cable		
		Temperature Vs. Time		
Job No: CAPR003066	Hone Bay	Date:	Approved:	Figure:
Filename: App_A_SD_GTC.pptx	поре Бау	Jan 2025	PDL	A.45

## **ID-GTC-3**

• Recent Interim Dike Ground Temperature Cable data were collected interchangeably via data logger and manual



CAPR003066 Job No: Hope Bay Filename: App\_A\_SD\_GTC.pptx

Date: Jan 2025

Approved: PDL

gure: A.46

Appendix B Thermosyphons


Appendix C Datalogger Battery Levels





Appendix D Inclinometers

		Inclinometers Measured			ured			
	Date	070-1	070-2	070-3	120-1	120-2	120-3	Comments
	Sep-2023							
ſ	Oct-2023							
ſ	Nov-2023							
ſ	Dec-2023							
ſ	Jan-2024							
ſ	Feb-2024							
ſ	Mar-2024							
ſ	Apr-2024							
ſ	May-2024							
ſ	Jun-2024							No measurements provided (120-1, 120-2, 120-3)
ſ	Jul-2024							Two surveys provided on July 11 and July 20, 2024 (120-1, 120-2, 120-3)
Ī	Aug-2024							
Ī	Sep-2024							Error measurements (check sum values above threshold) were noted. These measurements a
– L								

#### Notes:

1.

Green indicates good quality inclinometer survey data Orange indicated poor quality inclinometer survey data, or data where collection issues were noted Grey indicates that no survey data was collected

2. 3.

	srk consulting	
	0	AGNIC
Job No:	CAPR003066	Но
Filename:	App_U_inclinometers.pptx	







20-09-11         20-11-19         21-01-20         21-06-09         21-08-14         21-10-02         21-12-11         22-02-11         22-04-25         22-06-24         22-08-20         22-10-08         23-04-28         23-06-15         23-09-24         23-11-05         24-01-05         24-03-10         24-07-20         24-09-10	2020-10-20 2020-12-23 2021-02-20 2021-07-11 2021-09-04 2021-11-13 2022-03-27 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-07-25 2022-09-18 2022-07-25 2022-09-18 2023-05-08 2023-05-08 2023-07-14 2023-10-10 2023-10-10 2024-04-06 2024-04-06 2024-08-19 2024 TIA AGI
120-09-11         120-11-19         121-01-20         121-06-09         121-08-14         121-10-02         121-12-11         122-02-11         122-04-25         122-04-25         122-08-20         122-10-08         123-04-28         123-04-28         123-04-15         123-04-28         123-04-28         120-05         124-01-05         124-05-03         124-05-03         124-07-20         124-09-10	2020-10-20 2020-12-23 2021-02-20 2021-07-11 2021-09-04 2021-11-13 2022-03-27 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-07-25 2022-09-18 2022-09-18 2022-11-04 2023-05-08 2023-05-08 2023-07-14 2023-10-10 2024-04-06 2024-04-06 2024-06-27 2024-08-19
120-09-11         120-11-19         121-01-20         121-06-09         121-08-14         121-10-02         121-12-11         122-02-11         122-04-25         122-04-25         122-04-25         122-04-25         122-04-25         122-04-25         122-04-25         122-04-25         122-04-25         123-04-28         123-04-28         123-09-24         123-11-05         124-01-05         124-03-10         124-05-03         124-07-20         124-09-10	2020-10-20 2020-12-23 2021-02-20 2021-09-04 2021-11-13 2022-03-27 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-09-18 2022-09-18 2022-05-08 2023-05-08 2023-05-08 2023-05-08 2023-10-10 2023-10-10 2023-12-02 2024-04-06 2024-06-27 2024-08-19
120-09-11         120-11-19         121-01-20         121-06-09         121-08-14         121-10-02         121-12-11         122-02-11         122-04-25         122-06-24         122-08-20         123-04-28         123-04-28         123-09-24         123-11-05         124-01-05         124-05-03         124-07-20	2020-10-20 2020-12-23 2021-02-20 2021-07-11 2021-09-04 2021-11-13 2022-03-27 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-09-18 2022-11-04 2023-05-08 2023-05-08 2023-07-14 2023-10-10 2023-10-10 2024-04-06 2024-08-19
120-09-11         120-11-19         121-01-20         121-06-09         121-08-14         121-10-02         121-12-11         122-02-11         122-04-25         122-06-24         122-08-20         122-10-08         123-04-28         123-06-15         123-09-24         123-09-24         123-11-05         124-01-05         124-03-10	2020-10-20 2020-12-23 2021-02-20 2021-07-11 2022-09-04 2022-01-17 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-09-18 2022-09-18 2022-11-04 2023-05-08 2023-05-08 2023-07-14 2023-10-10 2024-04-06 2024-06-27
120-09-11         120-11-19         121-01-20         121-06-09         121-08-14         121-10-02         121-12-11         122-02-11         122-04-25         122-06-24         122-08-20         122-10-08         123-04-28         123-04-28         123-09-24         123-09-24         123-11-05         124-01-05	2020-10-20 2020-12-23 2021-02-20 2021-07-11 2022-09-04 2022-01-17 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-09-18 2022-09-18 2022-11-04 2023-05-08 2023-05-08 2023-07-14 2023-10-10 2023-10-10 2023-02-10 2023-02-10
120-09-11         120-11-19         121-01-20         121-06-09         121-08-14         121-10-02         121-12-11         122-02-11         122-04-25         122-06-24         122-08-20         122-10-08         123-04-28         123-09-24         123-09-24         123-09-24         123-11-05	2020-10-20 → 2020-12-23 2021-02-20 2021-09-04 2021-11-13 → 2022-01-17 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-09-18 2023-05-08 2023-07-14 2023-10-10 → 2023-12-02
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20-09-11 20-11-19 21-01-20 21-06-09 21-08-14 21-10-02 21-12-11 22-02-11 22-04-25 22-06-24 22-08-20 22-10-08 23-04-28 23-06-15	2020-10-20 2020-12-23 2021-02-20 2021-07-11 2021-09-04 2021-11-13 2022-01-17 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-09-18 2022-11-04 2023-05-08 2023-07-14
20-09-11 20-11-19 21-01-20 21-06-09 21-08-14 21-10-02 21-12-11 22-02-11 22-02-11 22-04-25 22-06-24 22-08-20 22-10-08 23-04-28	2020-10-20 2020-12-23 2021-02-20 2021-07-11 2021-09-04 2021-11-13 2022-03-27 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-11-04 2023-05-08
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20-09-11 20-11-19 21-01-20 21-06-09 21-08-14 21-10-02	2020-10-20 2020-12-23 2021-02-20 2021-07-11 2021-09-04 2021-11-13 2022-01-17
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20-09-11 20-11-19 21-01-20 21-06-09	2020-10-20 2020-12-23 2021-02-20 2021-07-11 2021-07-11
20-09-11 20-11-19 21-01-20	→ 2020-10-20 → 2020-12-23 → 2021-02-20
20-09-11 20-11-19	2020-10-20
20-09-11	2020-10-20
20.00.44	
20-07-12	2020-08-08
20-03-10	2020-06-06
20-01-16	
19-10-26	
19-08-25	2019-09-28
19-06-11	2019-07-27
19-04-14	2019-05-10
19-01-25	2019-01-01
18-11-10	2010-10-21
18-07-07	2018-08-03
18-05-19	2018-06-08
18-03-21	2018-04-20
18-01-16	2018-02-16
17-11-16	2017-12-16
17-09-14	2017-10-14
17-07-16	
17-05-20	
17-03-23	2017-04-15
17-01-26	
16-11-26	
16-08-14	<del>~~</del> 2016-09-25
16-04-11	
16-02-08	2016-03-07
15-11-25	
15-09-04	<u>→</u> 2015-10-09
15-07-09	
15-05-18	
15-02-02	
14-09-01 15-02-02	
14-07-12	
13-10-01	
12 10 01	
9/2012 X	
13-10-01	2013-07-26 



itial Reading (9/8/2012)	<b></b> 9/9/3	2012 X	
9/2012 X		-07-26	
)13-10-01	<b>——</b> 2014	-05-18	
)14-07-12	<del>~~</del> 2014	-08-08	
)14-09-01	<del></del> 2014	-10-01	
15-02-02	<b>—</b> 2015	-03-21	
15-04-08	<b>—</b> 2015	-04-16	
)15-05-18		-06-25	
)15-07-09	2015	-08-02	
15-09-04	<del>~~</del> 2015	-10-09	
)15-11-25		-12-30	
16-02-08		-03-07	
)16-04-11	2016	-07-02	
16-08-14	<del>~~</del> 2016	-09-25	
)16-11-26		-12-24	
)17-01-26	<b>——</b> 2017	-02-23	
)17-03-23	2017	-04-15	
)17-05-20	2017	-06-25	
)17-07-16	2017	-08-09	
)17-09-14	2017	-10-14	
)17-11-16	2017	-12-16	
018-01-16	2018	-02-16	
)18-03-21	2018	-04-20	
)18-05-19	2018	-06-08	
)18-07-07	2018	-08-03	
)18-09-29	2018	-10-21	
)18-11-10		-01-01	
)19-01-25		-02-14	
)19-04-14		-05-10	
)19-06-11		-07-27	
019-08-25		-09-28	
)19-10-26		-11-23	
020-01-16		-02-18	
020-03-10		-06-06	
020-07-12	2020	-08-08	
020-09-11		-10-20	
020-11-19		-12-23	
021-01-20		-02-20	
021-06-09	2021	-07-11	
021-08-14	2021	-09-04	
J21-10-02	2021	-11-13	
121-12-11	2022		
JZZ-UZ-11	2022		
JZZ-04-25	2022		
122-00-24	2022	-07-25	
122-08-20 122-10-08	2022	-09-18	
122-10-00 122 04 29	2022	-11-04	
123-04-20	2023		
123-00-13	2023	-07-14	
123-11-05	2023	-12-02	
024-01-05	2023	-02-10	
124-03-10	2024	-04-06	
24-05-03		-06-27	
)24-07-20	2024	-08-19	
24-09-10	~ 2027		
× .			
		2024 TIA AGI	
	Inc	linometer 07	0-1
		isplacement	s
Hope Bay	Date:	Approved:	Figure:
	Oct. 2024	PDL/AN	D.3



	2024 TIA AGI		
	Inclinometer 070-1A Displacement Time Series		
Норе Вау	Date: Oct. 2024	Approved: PDL/AN	Figure: D.4







# **Profile Parallel to Centerline**



Manufacture's accuracy is +/- 0.25 mm per location
 Survey data excluded from the charts is noted on Figure D.1



Initial Reading (9/8/2012) 2013-10-01 2014-07-12 2014-09-01 2015-02-01 2015-04-16 2015-06-25 2015-08-02 2015-09-04 2015-11-25 2016-02-08 2016-04-11 2016-08-14 2016-08-14 2016-08-14 2017-02-23 2017-04-15 2017-06-25 2017-08-09 2017-10-14 2017-12-16 2018-02-16 2018-02-16 2018-02-16 2018-02-16 2018-04-20 2018-06-08 2018-08-03 2018-10-21 2019-01-01 2019-02-14 2019-05-10 2019-07-27 2019-09-28 2019-01-23 2020-02-18 2020-06-06 2020-08-08 2020-08-08 2020-10-20 2021-07-11 2021-09-04 2021-07-11 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-01-17 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-01-17 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-01-17 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-01-17 2022-03-27 2022-05-16 2022-07-25 2022-09-18 2022-01-17 2023-05-08 2023-07-14 2023-05-08 2023-07-14 2023-05-08 2023-07-14 2023-02-10 2024-02-10 2024-02-10 2024-02-10 2024-02-10	<pre>&gt;&gt; 2013-07-26</pre>
2024-04-06 2024-06-27 2024-09-07	

	2024 TIA AGI		
	Inclinometer 070-2 Profiles		
Норе Вау	Date: Oct. 2024	Approved: PDL/AN	Figure: <b>D.6</b>



<ul> <li>Initial Reading (9/8/2012)</li> <li>2013-10-01</li> </ul>	─ <del>──</del> 2013-07-26 ─ <del>↓</del> ─ 2014-05-20
	<b></b> 2014-10-01
<u> </u>	
	2015-07-09
<u>~~</u> 2015-08-02	
	<b></b> 2015-12-30
	<b>——</b> 2016-09-26
<b></b> 2016-11-26	
2017-06-25	<b>—4</b> —2017-07-16
2017-08-09	2017-09-14
2017-10-14	2017-11-16
2017-12-16	2018-01-16
2018-02-16	
2018-04-20	
2018-06-08	
2018-08-03	
2019-05-10	
2019-07-27	
2019-09-28	2019-10-26
2019-11-23	2020-01-16
2020-02-18	
	2020-07-12
2020-08-08	2020-09-11
2020-10-20	2020-11-19
2020-12-23	
2021-02-20	2021-00-05
2021-09-04	
2022-01-17	2022-02-10
	2022-04-25
2022-05-16	2022-06-24
2023-05-08	2023-06-15
2023-07-14	
	2024-01-05
2024-02-10	2024-03-10
	<b>—</b> — <b>2024-08-19</b>
2024-09-07	
	2024 TIA AGI

	2024 TIA AGI Inclinometer 070-2 Displacements		
Hope Bay	Date: Oct. 2024	Approved: PDL/AN	Figure: <b>D.7</b>









Manufacture's accuracy is +/- 0.25 mm per location
 Survey data excluded from the charts is noted on Figure D.1



**       2013-10-01 $\leftarrow$ 2014-05-20         **       2014-09-01 $\leftarrow$ 2014-08-08         **       2015-02-01 $\leftarrow$ 2015-03-21         **       2015-06-25 $\leftarrow$ 2015-07-09         **       2015-08-02 $\leftarrow$ 2015-07-09         **       2015-07-09 $\leftarrow$ 2015-07-09         **       2015-07-09 $\leftarrow$ 2015-07-09         **       2015-07-02       2016-02-08       2016-02-08         2016-07-02 $\leftarrow$ 2016-02-08       2016-02-08         2016-07-02 $\leftarrow$ 2017-02-23 $\leftarrow$ 2017-02-23         *       2016-07-02 $\leftarrow$ 2017-04-15 $\leftarrow$ *       2017-07-16 $\leftarrow$ 2017-10-14 $2017-10-14$ 2017-07-16 $\leftarrow$ 2017-10-14 $2017-10-14$ $2017-01-14$ 2018-05-19 $\leftarrow$ 2018-06-08 $2018-06-08$ $2018-06-08$ 2018-05-19 $\leftarrow$ 2018-06-18 $2019-02-14$ $2019-02-14$ 2019-01-25 $\leftarrow$ 2019-02-14 $2019-02-14$ $2019-02-14$ 2019-01-25 $\leftarrow$ 20	Initial Reading (9/9/2012)	
$\begin{array}{c ccccc} + & 2014 + 0.8 + 0.8 \\ \hline & 2014 + 0.9 + 0.1 \\ \hline & 2015 + 0.2 + 0.1 \\ \hline & 2015 + 0.0 + 0.1 \\ \hline & 2017 + 0.0 + 1 \\ \hline & 2018 + 0.1 + 0 \\ \hline & 2028 + 0.1 + 0 \\$		
$\begin{array}{c} 2014-09-01 \\ 2015-02-01 \\ 2015-03-21 \\ 2015-04-16 \\ 2015-06-25 \\ 2015-07-09 \\ 2015-08-02 \\ 2015-09-04 \\ 2015-11-25 \\ 2015-09-04 \\ 2015-11-25 \\ 2015-09-04 \\ 2015-11-25 \\ 2016-03-07 \\ 2016-04-11 \\ 2016-07-02 \\ 2016-08-14 \\ 2016-09-25 \\ 2017-01-22 \\ 2016-01-224 \\ 2017-02-23 \\ 2017-03-23 \\ 2017-03-23 \\ 2017-06-25 \\ 2017-07-16 \\ 2017-08-09 \\ 2017-09-14 \\ 2017-10-14 \\ 2017-10-14 \\ 2017-10-14 \\ 2017-10-14 \\ 2017-10-14 \\ 2017-10-14 \\ 2018-03-21 \\ 2018-03-21 \\ 2018-03-21 \\ 2018-04-16 \\ 2018-03-21 \\ 2018-04-16 \\ 2018-03-21 \\ 2018-04-16 \\ 2018-03-21 \\ 2018-04-16 \\ 2018-03-21 \\ 2018-04-15 \\ 2019-04-15 \\ 2019-01-25 \\ 2019-05-10 \\ 2019-06-12 \\ 2019-06-12 \\ 2019-07-27 \\ 2019-08-25 \\ 2019-07-27 \\ 2019-08-25 \\ 2019-07-27 \\ 2019-08-25 \\ 2019-07-27 \\ 2019-08-25 \\ 2019-07-27 \\ 2019-08-25 \\ 2019-01-25 \\ 2019-07-27 \\ 2019-08-25 \\ 2019-07-27 \\ 2019-08-25 \\ 2019-01-26 \\ 2020-07-12 \\ 2020-01-16 \\ 2020-02-18 \\ 2020-01-16 \\ 2020-02-18 \\ 2020-01-10 \\ 2020-01-20 \\ 2021-02-20 \\ 2021-02-20 \\ 2021-02-20 \\ 2021-02-20 \\ 2021-02-20 \\ 2021-02-20 \\ 2022-00-21 \\ 2022-00-20$	$\rightarrow$ 2010-10-01 $\rightarrow$ 2014-07-12	
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▲       2021-12-11       →       2022-01-17         ★       2022-02-10       ▲       2022-03-28         2022-04-25       2022-05-16         2022-08-20       ↓       2022-09-18         ★       2022-04-28       2022-09-18         2023-06-15       2023-05-12       2023-05-12         2023-06-15       2023-09-24       ∠         ▲       2023-08-11       ▲       2023-09-24         ▲       2023-08-11       ▲       2023-09-24         ▲       2023-10-10       ★       2023-11-04         ★       2023-12-02       ▲       2024-01-07         ↓       2024-02-11       2024-03-10         ∠024-02-11       ∠024-05-04       ↓         ↓       2024-06-27       ↓       2024-08-19         ↓       2024-09-07       ↓       2024-08-19		
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2022-10-08       2022-11-04         2023-04-28       2023-05-12         2023-06-15       2023-07-14         2023-08-11       2023-09-24         2023-10-10       2023-11-04         2023-12-02       2024-01-07         2024-02-11       2024-03-10         2024-04-06       2024-05-04         2024-06-27       2024-08-19         2024-09-07       2024-08-19		
2023-04-28       2023-05-12         2023-06-15       2023-07-14         2023-08-11       2023-09-24         2023-10-10       2023-11-04         2023-12-02       2024-01-07         2024-02-11       2024-03-10         2024-04-06       2024-05-04         2024-06-27       2024-08-19         2024-09-07       2024-08-19		
2023-06-15       2023-07-14         2023-08-11       2023-09-24         2023-10-10       2023-11-04         2023-12-02       2024-01-07         2024-02-11       2024-03-10         2024-04-06       2024-05-04         2024-06-27       2024-08-19         2024-09-07       2024-08-19		2023-05-12
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	2024 TIA AGI		
	Inclinometer 070-3 Profiles		
Hope Bay	Date: Oct. 2024	Approved: PDL/AN	Figure: D.10



# **Displacement Parallel to Centerline**



-8 -8  $\rightarrow$ -0 -0 -0 --8- $\rightarrow$ 

Manufacture's accuracy is +/- 0.25 mm per location
 Survey data excluded from the charts is noted on Figure D.1



	Inclinemator 070.2
	2024 TIA AGI
2024-09-07	
2024-06-27	
2024-04-06	
2024-02-11	2024-03-10
-2023-12-02	
-2023-10-10	2023-11-04
-2023-08-11	2023-09-24
-2023-06-15	2023-07-14
-2023-04-28	2023-05-12
-2022-10-08	
-2022-08-20	
-2022-04-23	
-2022-02-10	2022-05-16
-2022-02-10	
-2021-12-11	2022-01-17
-2021-10-03	
-2021-08-14	2021-09-04
-2021-06-09	2021-07-11
-2021-01-20	
-2020-03-11	2020-10-20
-2020-07-12	2020-00-00
-2020-03-10	2020-00-00
-2020-01-10	
<u> </u>	2010-11-23
-2019-00-25	2019-09-28
- 2019-08-25	2013-07-27
<u> </u>	2019-07-27
-2019-01-25	2019-02-14
-2010-11-10	2019-01-01
-2010-09-29	2010-10-21
-2018-07-07 -2018-00-20	2018-03-03
-2018-02-19	
-2018-03-21	2018-04-20
- 2018-01-16 - 2018-02-21	2018-02-16
-2017-11-17	2017-12-16
-2017-09-14	2017-10-14
-2017-07-16	2017-08-09
- 2017-05-20	2017-06-25
-2017-03-23	
- 2016-12-24	
-2016-09-25	2016-11-26
-2016-07-02	2016-08-14
-2016-03-07	2016-04-11
-2015-12-30	
- 2015-10-09	2015-11-25
-2015-08-02	
-2015-06-25	
- 2015-04-16	
- 2015-02-01	
- 2014-09-01	
- 2014-07-12	<u> </u>
- 2013-10-01	
– Initial Reading (9/9/2012)	2013-07-26

	Inclinometer 070-3 Displacements		0-3 s
Hope Bay	Date:	Approved:	Figure:
	Oct. 2024	PDL/AN	D.11









AGN

Initial Reading (9/8/2012)	
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2017-05-20	2017-04-15
2017-03-20	2017-00-23
2017-07-10	2017-08-09
2017-09-14	2017-10-14
2017-11-17	2017-12-10
2018-01-16	2018-02-16
2018-03-21	2018-04-20
2018-05-19	2018-06-08
2018-07-07	2018-08-03
2018-09-29	2018-10-21
2018-11-10	2019-01-01
2019-01-28	2019-02-16
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2019-11-24	2020-01-20
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2024-07-20	
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$\checkmark$		2024 TIA AGI	
	Inclino	meter 120-1 F	Profiles
Норе Вау	Date: Oct. 2024	Approved: PDL/AN	Figure: <b>D.14</b>





**Displacement Parallel to Centerline** 

Depth (m)

Manufacture's accuracy is +/- 0.25 mm per location
 Survey data excluded from the charts is noted on Figure D.1



# LEGEND:

<ul> <li>Initial Reading (9/8/2012)</li> <li>2013-08-28</li> <li>2014-05-20</li> <li>2014-08-08</li> <li>2014-10-01</li> <li>2015-03-21</li> <li>2015-07-09</li> <li>2015-07-09</li> <li>2015-09-04</li> <li>2015-11-25</li> <li>2016-07-02</li> <li>2016-07-02</li> <li>2016-07-02</li> <li>2016-12-24</li> <li>2017-03-23</li> <li>2017-05-20</li> <li>2017-07-16</li> <li>2017-09-14</li> <li>2017-09-14</li> <li>2017-01-6</li> <li>2018-01-16</li> <li>2018-01-16</li> <li>2018-01-16</li> <li>2018-05-19</li> <li>2018-07-07</li> <li>2018-07-07</li> <li>2018-01-16</li> <li>2019-04-15</li> <li>2020-02-18</li> <li>2020-02-20</li> <li>2021-02-20</li> <li>2021-02-20</li> <li>2021-02-20</li> <li>2021-02-20</li> <li>2022-03-28</li> <li>2022-01-18</li> <li>2022-03-28</li> <li>2022-01-18</li> <li>2022-01-18</li> <li>2022-01-18</li> <li>2022-01-18</li> <li>2022-01-18</li> <li>2022-01-25</li> <li>2022-01-25</li> <li>2022-01-26</li> <li>2022-01-26</li> <li>2022-01-26</li> <li>2022-01-26</li> <li>2022-01-26</li> <li>20</li></ul>	<ul> <li>2013-07-26</li> <li>2014-07-12</li> <li>2014-09-01</li> <li>2015-02-02</li> <li>2015-04-16</li> <li>2015-06-25</li> <li>2015-08-02</li> <li>2015-10-09</li> <li>2015-12-30</li> <li>2016-04-11</li> <li>2016-08-14</li> <li>2016-01-126</li> <li>2017-02-23</li> <li>2017-04-15</li> <li>2017-02-23</li> <li>2017-06-25</li> <li>2017-06-25</li> <li>2017-06-25</li> <li>2017-014</li> <li>2017-10-14</li> <li>2017-12-16</li> <li>2018-06-08</li> <li>2018-06-08</li> <li>2018-06-08</li> <li>2018-06-08</li> <li>2018-06-08</li> <li>2019-02-16</li> <li>2019-02-16</li> <li>2019-02-16</li> <li>2019-07-27</li> <li>2019-09-28</li> <li>2020-01-20</li> <li>2020-01-20</li> <li>2020-03-12</li> <li>2020-07-12</li> <li>2020-09-11</li> <li>2020-01-20</li> <li>2021-06-09</li> <li>2021-06-09</li> <li>2021-06-09</li> <li>2021-06-09</li> <li>2022-02-10</li> <li>2022-02-10</li> <li>2022-04-29</li> <li>2022-04-29</li> <li>2022-04-29</li> <li>2022-04-29</li> <li>2022-04-28</li> <li>2023-04-28</li> <li>2023-04-28</li> <li>2023-04-11</li> </ul>
2023-09-24	2023-10-10
2024-01-07	2024-02-12
	2024-04-06
2024-05-04	2024-07-11
2024-07-20	2024-08-31
2024-09-07	
	2024 TIA AGI

	Inclinometer 120-1 Displacements		0-1 s
Hope Bay	Date:	Approved:	Figure:
	Oct. 2024	PDL/AN	D.15









Manufacture's accuracy is +/- 0.25 mm per location
 Survey data excluded from the charts is noted on Figure D.1



Initial Reading (0/8/2012)	
~ 1110a Neaulig (3/0/2012)	
2014-05-20	2014-07-12
- 2014-10-01	
← 2015-03-21	2015-04-16
₩ 2015-04-20	<b>——</b> 2015-05-19
- 2015-06-26	
- 2015-08-02	<del>~~</del> 2015-09-04
- 2015-10-09	
	2016-04-11
-2016-07-02	2016-08-14
-2016-09-25	
2016-11-26	
2017_02_22	2017-02-25
- 2017-03-23	
2017-05-20	2017-00-25
2017-07-16	2017-08-09
2017-09-14	2017-10-14
2017-11-17	2017-12-16
2018-01-16	2018-02-17
	2018-04-20
	2018-06-08
2018-07-07	2018-08-03
	2018-10-21
2018-11-10	2019-01-01
	2019-04-15
-2019-05-10	2019-06-12
2019-07-27	2019-08-25
2010-00-28	2010-10-26
2019-05-28	2013-10-20
2019-11-24	
2020-02-18	2020-05-12
2020-06-06	2020-07-12
2020-08-08	2020-09-11
2020-10-20	
2020-12-24	<b>→</b> 2021-01-20
-2021-02-20	2021-06-09
2021-07-11	2021-08-14
2021-09-04	
2021-11-15	
-2022-01-18	<del>——</del> 2022-02-10
2022-03-28	2022-04-29
2022-05-16	2022-06-24
2022-07-25	
2022-09-18	2022-00-20
2022-05-10	2022 10 00
2023-03-13	
2023-07-14	
	2023-10-10
2023-11-04	
2024-01-07	2024-02-11
2024-03-14	2024-04-06
2024-05-04	2024-07-11
2024-07-20	
2024-09-07	

$\checkmark$		2024 TIA AGI	
	Inclino	meter 120-2 F	Profiles
Hope Bay	Date: Oct. 2024	Approved: PDL/AN	Figure: <b>D.18</b>





# **Displacement Parallel to Centerline**

Depth (m)

50

Manufacture's accuracy is +/- 0.25 mm per location
 Survey data excluded from the charts is noted on Figure D.1



Initial Reading (9/8/2012)	<b>—</b> 2013-07-26
<del>←</del> 2013-08-28	<del>———</del> 2013-10-01
- 2014-05-20	<u> </u>
2014-08-08	<b>—</b> 2014-09-01
- 2014-10-01	
← 2015-03-21	
-2015 05 21 -2015 04-20	
2015-04-20	2015-03-15
	2015-07-09
2015-06-02	2015-09-04
2015-10-09	2015-11-25
	2016-04-11
	2016-08-14
- 2017-03-23	
	2017-06-25
	2017-08-09
	2017-10-14
2017-11-17	2017-12-16
2018-01-16	2018-02-17
	2018-04-20
-2018-05-19	2018-06-08
2018-07-07	2018-08-03
2018-09-30	2018-00-00
2018-05-50	2010 10 21
2010-11-10	2019-01-01
2019-01-25	2019-04-13
2019-03-10	2019-00-12
2019-07-27	2019-08-25
2019-09-28	2019-10-26
2019-11-24	2020-01-20
- 2020-02-18	
2020-06-06	2020-07-12
2020-08-08	2020-09-11
2020-10-20	
2020-12-24	<b>→</b> 2021-01-20
-2021-02-20	
2021-07-11	2021-08-14
2021-09-04	
2021-11-15	
-2022-01-18	<del>——</del> 2022-02-10
-2022-03-28	2022-04-29
2022-05-16	2022-06-24
2022-07-25	
2022-09-18	2022-10-08
2022-11-05	
2023-05-13	2023-06-16
2023-07-14	2023 00 10
2023-07-14	2023-00-11
2023-03-24	
	2024-02-11
2024-03-14	2024-04-06
2024-05-04	2024-07-11
2024-07-20	2024-08-31
2024-09-07	

		2024 TIA AGI	
	Inclinometer 120-2 Displacements		
Норе Вау	Date: Oct. 2024	Approved: PDL/AN	Figure: <b>D.19</b>

**Inclinometer 120-2A Timeseries** 25.00 20.00 15.00 Horizontal Displacement (mm) 10.00 5.00 0.00 -5.00 -10.00 12/27/2014 9/22/2017 11/18/2010 4/1/2012 8/14/2013 5/10/2016 2/4/2019 6/18/2020 10/31/2021 3/15/2023 Date ND-IN-120-3 ND-IN-120-1 ND-IN-120-1 Notes: Manufacture's accuracy is +/- 0.25 mm per location
 Survey data excluded from the charts is noted on Figure D.1 

Filename: App\_D\_Inclinometers.pptx

Job No: CAPR003066





Filename: App\_D\_Inclinometers.pptx

	2024 TIA AGI		
	Incl	inometer 120	)-2A
	Velo	ocity Time Se	ries
Hope Bay	Date:	Approved:	Figure:
	Oct. 2024	PDL/AN	D.21









200

Manufacture's accuracy is +/- 0.25 mm per location
 Survey data excluded from the charts is noted on Figure D.1



# LEGEND:

	Inclinometer 120-3 Profiles
<u>→</u>	2024 TIA AGI
2024-07-11	
2024-02-11	2024-03-14
	2024-01-07
	<del>~~~</del> 2023-11-04
2023-06-16	
2023-04-28	2023-05-13
2022-08-20	2022-09-18
2022-06-24	
2022-04-29	
	2022-03-28
→ 2021-12-11	<u> </u>
	2021-11-15
2021-08-14	<b>2021-09-04</b>
2021-06-09	
	→ 2021-02-20
2020-11-19	
2020-09-11	2020-10-20
<b>2020-07-12</b>	
2020-03-12	→ 2020-06-06
-2010 10-20	
2019-10-26	
2019-00-12	2019-09-28
2019-04-13	2019-03-10
2019-01-01	2013-01-23
2010-10-21	
2018-00-03	2018-09-29
2018-04-20	2018-05-19
2018-02-17	2018-03-21
2017-12-16	2018-01-17
2017-10-14	2017-11-17
2017-08-09	2017-09-14
2017-04-15	2017-05-20
→ 2017-01-03	2017-01-26
2016-09-25	<b>—</b> 2016-11-26
2016-07-02	2016-08-14
2016-03-07	
2015-12-30	
2015-08-28	<b></b> 2015-09-04
	<del></del> 2015-08-02
	─ <del>──</del> 2015-06-26
	2015-02-02
- Initial Poading (0/8/2012)	

Date: Oct. 2024

Approved: PDL/AN

Figure: D.22



	Inclinometer 120-3
$\mathbf{i}$	2024 TIA AGI
2024-00-31	2024-03-07
2024-07-11	2024-07-20
2024-04-07	
2024-02-11	
	2024-01-07
2023-10-10	
2023-06-16	
2022-00-24	
2022-04-29	
	2022-03-28
2021-12-11	<u> </u>
2021-08-14	
2021-06-09	
2021-01-20	2021-02-20
2020-11-19	
2020-09-11	2020-10-20
<b>2020-07-12</b>	
2020-03-12	→ 2020-06-06
2019-10-26	2019-11-24
	2019-09-28
	2019-07-27
2019-04-15	2019-05-10
2019-01-01	2019-01-25
	2018-11-10
2018-08-03	2018-09-29
2018-06-08	2018-07-07
2018-04-20	2018-05-19
2018-02-17	2018-03-21
2017-12-16	2018-01-17
2017-10-14	2017-11-17
2017-08-09	
2017-04-15	2017-05-20
<del>→</del> 2017-01-03	
2016-09-25	<b>——2016-11-26</b>
2016-07-02	2016-08-14
2016-03-07	2016-04-11
	2016-02-08
	<b></b> 2015-11-25
2015-08-28	<b>—4</b> 2015-09-04
	<b>—+—</b> 2015-08-02
	<del>~~</del> 2015-06-26
	— <del>—</del> 2015-02-02
<del>~~</del> 2014-08-08	
2014-05-20	<b>—</b> 2014-06-18
Initial Reading (9/8/2012)	2013-07-26

	Inclinometer 120-3 Displacements		
Норе Вау	Date:	Approved:	Figure:
	Oct. 2024	PDL/AN	D.23





Appendix E Survey Monitoring



CAPR003066 Job No:

Filename:

DORIS TIA

App\_E\_SurveyMonitoring.pptx

Displacement Time		
Date: Oct. 2024	Approved: PDL/AN	





Filename: App\_E\_SurveyMonitoring.pptx

5. The latest data were received on August 11, 2024

DORIS TIA

proved: PDL/AN

Figure E.2







	2024 TIA AGI			
	Surficial Survey Monitoring Points Displacement Timeseries			
ORIS TIA	Date: Oct. 2024	Approved: PDL/AN	Figure: E.5	




	2024 TIA AGI			
	Crest Survey Monitoring Points Displacement Timeseries			
OORIS TIA	Date: Oct. 2024	Approved: PDL/AN	Figure: E.7	

Appendix F TIA Reclaim Pond Water Levels





Appendix G Climate Data





## Note:

- Mean daily values measured at Doris Meteorological Station 1.
- Data record from February 2004 to October 2024 2.





Note:

1. Doris meteorological station air temperature plotted year of year

2. Mean annual air temperature based on thermal year period (Oct. 1 to Sep. 30)



	Mean Annual Air		
ear	Temperature (°C)		
05	-12.5		
06	-9.1		
07	-10.8		
08	-12.6		
09	-11.3		
10	-8.6		
11	-9.8		
12	-9.9		
13	-11.0		
14	-11.2		
15	-10.7		
16	-10.1		
17	-9.4		
18	-11.8		
19	-11.3		
20	-9.7		
21	-10.8		
22	-9.5		
23	-9.8		
24	-7.8		
rage	-10.4		

N 1					
	2024 TIA AGI				
	Air Temperature				
IICO EAGLE					
Hope Bay	Date:	Approved:	Figure:		
	Dec, 2024	CWS	۷		



Note:

1. Freezing and thaw degree days calculated from mean daily air temperature for thermal year period (Oct. 1 to Sep. 30)



	2024 TIA AGI			
	Freezing and Thawing Degree Days			
Hope Bay	Date: Dec, 2024	Approved: CWS	Figure: 3	-